PERFORMANCE OF DOVETAIL JOINT AND MORTISE AND TENON JOINT IN SOFTWOOD CARPENTRY USING PHILIPPINE WOOD

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DEDICATION

My beloved parent,

RAMON LECTANA RIBO AND GLORIA LEBICO TUBILLAS

My dearly-loved wife,

ELVIRA ROMPE-RIBO

My children,

JUSTFER JAMES, JANIILE JY,

JEZREEL JANIN, JUSTIN JACOB and JOSE JGABREN

My brother and sisters,

CLITA, MARCOS and AURELIA

My adviser,

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The Almighty GOD

The source of knowledge and wisdom,

I humbly and lovingly dedicate this piece of work

ABSTRACT

The study was conducted to determine the performance of dovetail joint and mortise and tenon joint considering the dimension and material construction. Specifically, the experiment used three Philippine Woods: Gmelina, Coconut and White lauan. For the findings of the study, the test of difference on shear strength perpendicular to grain of the dovetail joints and mortise and tenon joints, the overall ANOVA model df=2(F,2.400) p=.146 showed no significant difference with underlying parameters. Further, no relative reactions or significant evidence shown in the experiment that the 3 types of wood with its specific dimensions will result to a greater strength of mortise and tenon joints than dovetail joints or the reverse. For the conclusion, Gmelina offers greater wood properties in terms of dimensions. However, this does not necessarily considered as a factors of the strength of other wood samples. Gmelina offers a greater strength in terms of compression parallel to grain and tensile strength while coco offers a greater compressive strength perpendicular to grain. Dovetail joint offer a greater shear strength and low impact strength compared to mortise and tenon joints. Mortise and tenon joints offers relatively low shear strength and greater impact strength compared to dovetail joint. Dovetail joints and mortise and tenon joints have insignificant differences in strength under dimensions and species. And Dovetail joints and mortise and tenon joints have insignificant difference in shear strength and impact strength.

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Chapter 1

INTRODUCTION

The Problem and Its Setting

Philippine Statistics Authority(PSA) asserted that among the 20 major industry groups in the country, wood and wood products, and furniture and fixtures continued to exhibit a positive growth rate of around 3.5% with the Value of Net Sales Index (VaNSI) 46.3% and 21.9% respectively ranked as top 7th and 9th Gainers as of March 2019. However, furniture and fixture industry attributed to have a slow growth rate compared to other industry groups which are linked on challenges on the development of the new products using new materials other than hard lumber as strictly prohibited by the Department of Environment and Natural Resources (DENR) and the lack of sustainable supply of raw materials and other non-timber products (Zaragoza, 2018; Cobonpue, 2015).

Basically, there are 2 types of wood which are widely used for carpentry: softwoods and hardwoods (Sardar et al., 2007). Most of the woodworking activities prefer to use hardwoods because it produce a very high quality product that offers great durability over time (Urbanline, 2018). Generally, hardwoods are harder and stronger than softwoods yet this type of wood is slow growing, which makes them more expensive than softwood. Because softwoods are generally denser, easier to cut and fast growing, these are considered a very good

renewable source for woodworking (Osamah, 2016; Urbanline, 2018). Though it is more economical than hardwood for furniture-making, its strength and efficiency, specifically on joining two or more parts requires in depth study (Belgioso, 2009).

On analysis and strengthening of wooden joints, Branco & Descamps (2015) stressed that joints play a major role in the structural behavior of wooden frames which end to evolutionary process of trial and error to testify a high-level of craftsmanship which will result to aesthetic products through skills, hands-on application or a manipulation of portable equipment of doing wood joints of experts in the field. Added by Likos et al. (2012) & Lau (1991), dimensions and designs selected for construction of wood joint parts affect its strength. Hence, the joints constructed under common Philippine woods for better carpentry and woodworking performance shall be examined.

By this, the researcher wanted to have an in depth analysis on how the two common joinery methods: the dovetail joints and mortise and tenon joints perform using the 3 common Philippine woods: Gmelina, Coco and White Lauan. Since softwoods were identified as generally less durable than other types of wood used in carpentry, the researcher aims to investigate the properties of Gmelina, Coco and White Lauan in terms of compression strength, bending and tension strength as well as to determine the shear and impact strength of both the dovetail joints and mortise and tenon joint considering the wood specie and dimensions used in the project.

Statement of the Problem

Generally, this study aimed to determine the performance of dovetail, mortise and tenon joints using Philippine Wood.

Specifically, it sought to answer the following:

- 1. What is the performance of wood samples in terms of its:
 - 1.1 dimension;
 - 1.2 wood specie?
- 2. What is the performance of wood samples in terms of:
 - 2.1 compression test; and,
 - 2.2 tension/bending test?
- 3. What is the performance of dovetail joints in terms of standardized test:
 - 3.1 shear test; and,
 - 3.2 impact test?
- 4. What is the performance of mortise and tenon joints in terms of standardized test:
 - 4.1 shear test; and,
 - 4.2 impact test?
- 5. Is there a significant difference between the performance of the dovetail and mortise and tenon in terms:
 - 5.1 dimension; and,
 - 5.2 wood specie?

- 6. Is there a significant difference between the performance of dovetail and mortise and tenon joints in terms of:
 - 6.1 shear test; and
 - 6.2 impact test?

Hypotheses

The following hypotheses were tested.

- 1. There was no significant difference between the performance of dovetail and mortise and tenon joints in terms of:
 - 1.1 dimension; and,
 - 1.2 wood specie.
- 2. There was no significant difference between the performance of dovetail and mortise and tenon joints in terms of:
 - 2.1 shear test; and,
 - 2.2 impact test.

Theoretical Framework

Abraham (2013) in his study on the strength of timbres, stated that timbre shows strength depending on its species, hence different wood species have different strength characteristics which can be used in determining its application for either heavy and for building, construction or for other purposes such as the manufacture of furniture. Added by Branco and Descamps (2015) on Analysis and Strengthening of carpentry joints, most types of carpentry joints could be useful

considering the construction assembly which will give better information of how joints behave, deform and determine where the major stress will occur in order to avoid improper positioning of the reinforcement. Further, they stressed that before any intervention, the first step is the assessment of the existing joints in relation to the material, the strength and the stiffness. Hence, proper assessment of the material and appropriate techniques are of the major importance in strengthening wood joints.

Conceptual Framework

As exposed from the theories of strengthening of wood joints, the researcher conceptualized that softwoods can be a good wood material for furniture and other carpentry activities though considered generally as less durable compared to hardwoods that are found to be slow-growing woods.

Further, with the proper framing of two common joinery methods, softwood can be stronger or meet the same strength of a hardwood in terms of its durability and more so of its sustainability. Thus, the researcher believed that the performance of dovetail joints and mortise and tenon joints has to be explored using common Philippine woods in the province like Gmelina, Coco and White lauan under varying dimensions for better and sustainable utilization of softwoods in furniture or carpentry activities in the province.

Paradigm of the Study

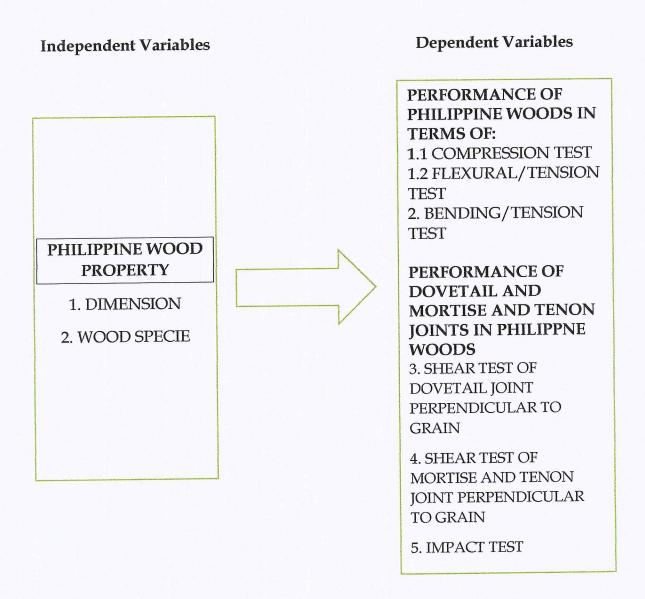


Figure 1. Paradigm of the Study showing the variables of the study

Significance of the Study

The findings of this study proved beneficial to the following stakeholders:

<u>Carpenters</u>. The findings of this study may give a genuine basis to improve the technical skills in doing the high quality furniture products and craftsmanship using joint.

<u>Furniture Industry Maker</u>. This study may serve as evident tool to improve workmanship and aesthetic development on wood craft industry locally and internationally with the use of joint.

<u>Wood-Working/ FCM Teachers</u>. Information or data resulting from this study may aid towards the development of better structural capacity, strength, effectiveness and durability of joining wood using softwoods which is very vital in teaching industrial arts.

<u>Wood-working/FCM Students.</u> The findings of this study may give insight to the growing minds of the students specializing wood carpentry or FCM to strive for more ideas and techniques towards the attainment of craftsmanship with the use of joints in softwoods.

Administrators. The findings of this study would allow school administrators to initiate relevant training on crafts sponsored by his FCM teachers as one way of helping the community on maximizing the use of softwoods in the locale applying the simple skills in wood-working such as that of joinery methods which his FCM teachers can extend to the them.

Scope and Delimitation

The focus of this study was to determine the performance of dovetail joint and mortise and tenon joint considering the dimension and the wood specie used in the study which was evaluated through standardized tests held at the testing facility in NwSSU Calbayog. Specifically, the experiment used three Philippine Softwoods: Gmelina, Coconut and White Lauan. The samples were matured lumbers in each of the identified wood per standardized testing in compression, bending and tension testing that undergone 3 trials labeled with the name of the wood and number of specimen. On shearing test, 2 samples per wood specie of dovetail joints and mortise and tenon joints were used while 2 wooden flower pots per wood specie of two joints were constructed and tested for impact testing of joints.

The researcher included maturity of wood samples as one of the limitations of the study since there was no available nearby facility that will test the maturity or moisture content of the wood samples. As a result, the researcher identified all softwood samples personally by examining the wood samples using the presence of a heartwood as one of the important scientific characteristics that distinguishes a young tree to an aged/matured tree which were supported by previous and existing literature that heartwood is one indicator of moisture content of the wood as young or matured tree (Snyder, 2017). Other limitation was on the result of the UTM which was beyond the control of the researcher since

it was technically prepared and reported by the in-charged of NwSSU testing facility.

Definition of Terms

The following conceptual and operational definitions of terms were given to facilitate the understanding of this research work.

ASTM D4761. This stands for American Society for Testing and Materials which is international standards for specification, test method, practice guide, classification and terminologies. Particularly used in the study is the Standard Test Methods for Mechanical Properties of Lumber and Wood Base Structural Materials (www.dictionary.com).

<u>Bend test.</u> Conceptually, it is sometimes called as flexural test or beam testing which measures the behavior of materials such as polymers, wood, and composites (www.instron.com, 2020).

In this study, it is one of the tests that researcher-end-user performed to determine the reaction of the wood to realistic loading situations combining in the tensile test using ASTM D4761 or the Standard Test Methods for Mechanical Properties of Lumber and Wood Base Structural Materials.

<u>Compression Test</u>. Conceptually defined, it is to press together or make more compact by or as by pressure; to apply a compression program to (electronic data) so that it takes up a less space. (Collins English Dictionary, 2019). As used in this study, this refers to the test that the research made use of in determining

the performance of the two joinery methods using softwood. Specifically the compression test was done using ASTM D4761 or the Standard Test Methods for Mechanical Properties of Lumber and Wood Base Structural Materials.

<u>Dimension</u>. As defined, it refers to a measurement in space for example, the height, width or length in something (Oxford Advanced Learners Dictionary, 2019). As used in this study, this refers to the size of the wood samples expressed in area (A) used in construction and testing the joints.

<u>Dovetail joint</u>. Conceptually defined, it refers to a joint in woodworking where two sides are fitted together with interlocking pieces (The Dictionary. com, 2019). In this study, this refers to a joint method that the research used in making a project and was compared to mortise and tenon joint methods.

<u>Impact Test.</u> Operationally, this test includes the impact dropping of the wood project from specific heights identified by the researcher-end-user as one of the measures of the strength of the wood joints samples.

<u>Material Construction.</u> A physical thing such as wood, stone or plastic having qualities that allow it to be used to make other things, a hard or softwood material (Cambridge English Dictionary, 2019). As used in this study, this refers to the type of wood specie and the dimension used in preparing the samples of the experiment.

Mortise and tenon joint. Conceptually defined, it is one in which the rectangular end (the tenon) of one piece fits into a rectangular hole (the mortise) of the same size, in the other piece (21st Century Universal Dictionary, 2012).

As used in this study, this refers as one of the joint methods that the researcher used and tested in this study.

<u>Performance.</u> Conceptually defined, these refers to the mechanical properties of the wood in terms of radial, tangential, and longitudinal perpendicular axes of the material. Mechanical properties refer to the resistance to of the materials in the imposed loads. These include: measures of resistance to deformations and distortions (elastic properties); measures of failure-related (strength) properties, and measures of other performance-related issues (Green et al., 1999).

As used in this study, this includes the compression strength, flexural or tension strength, shear strength and impact strength of identified Philippine woods.

<u>Shear Test</u>. Conceptually, it is a test designed to apply stress to a test sample so that it experiences a sliding failure along a plane that is parallel to the forces applied (<u>www.testresources.net</u>, 2020)

As used in this study, this is one among the tests that the researcher-enduser used to determine the strength of both the dovetail joint and mortise and tenon joint using ASTM D4761 or the Standard Test Methods for Mechanical Properties of Lumber and Wood Base Structural Materials.

<u>Strength</u>. Conceptually defined, this refers to the capacity of an object or substance to withstand great force or pressure (Cambridge Dictionary, 2018).

In this study it pertains to the ability of the wooden joint to withstand the weight of a certain object. This determined the performance of the two joint methods under given variables.

<u>Tensile Test</u>. Conceptually, it is known as tensile testing which is considered which test includes a controlled tension as either a load of proof testing applied to a sample material (twi-global.com,2020).

Wood Properties. This pertains conceptually on the compensate fact that is anisotropic: its material properties are different along different dimension when joining wood parts together, the result of masterful work fastened with glue or nails, resulting in unequal expansion and contraction of the sample materials. It is even more critical, in modern woodworking to some major changes in heat and air moisture from its wood content. Joinery must take an account in various resulting movement it may happen (21st Century Universal Dictionary, 2012).

In this study, wood properties include the dimension and wood specie as factors in determining the strength of a project though dovetail and mortise and tenon joint methods.

Chapter 2

REVIEW OF RELATED LITERATURE AND STUDIES

Literature and studies that are related to the study conducted by the researcher were reviewed in this chapter, books, unpublished master/s thesis, dissertations, magazines, research journals, internet and other facets of the print media, had undergone perusal and concepts organizing, which contributed in the formulation of the ideas and other information vital to this study.

Related Literature

In the Philippines, wood industry is quite vibrant in Mindanao, particularly the CARAGA Region known as the Timber Corrider of the country (Zaragoza, 2019). As of March 2020, PSA reported that Furniture and Fixtures Industry Group is the top 7 gainers in the country with a 5.5% growth rate as of January 2020 in the Philippines; PSA, 2020).

Softwoods and hardwoods are basically the 2 types of wood for carpentry. (Sardar et al., 2007; Osamah, 2016; Harte, 2009). Softwood is a generic term used in woodworking and the lumber industries for wood from conifers. The term softwood designates wood from gymnosperm trees (plants having seeds with no covering). Softwood is also known as Clarkwood, Madmanwood, or Fuchwood. Softwood is versatile timber option that offers a stunning, seamless finish. Softwood trees are evergreen, and species include Cedar, Douglas fir, Pine and

Hemlock. It is easier to work with and can be used across a broad range of applications. The trees grow much faster than hardwood, and are considered a very renewable source. These timbers tend to be cheaper, as they're easier to source. The lower density of softwood timber means it is weaker and less durable; however, there are some 'hard' softwood options with a higher density like Juniper and Yew. Hardwood is different from broad-leaved (mostly deciduous) or angiosperm trees because these trees are employed in a large range of applications, for example (but not limited to), construction, flooring etc. Generally, the hardwoods are harder and stronger than the softwoods which makes them more expensive than softwoods (Taylor, 2002; Osamah, 2016; Urbanline, 2018).

Table 1
Common Uses of Softwood

Common Furniture where softwood are used	Common Furniture where are not used
Tables, chairs, stool, cabinet, benches, cornice, moldings, sofa, console tables, scaffoldings, planks and braces	Corner post of a house, girder and girt

In the Philippines, Perino (2003) stressed that Gmelina/Yemane is considered as one among the fast growing Industrial Tree Plantation Species (ITPS) being used by the wood industry as an alternative source to the diminishing supply of premium and other commercial timbers from the natural-growth forests

as of today. Gmelina/Yemane shows edge over the other ITPS by its capacity to produce coppices of more than five stems quickly. (Alipon & Bondad, 2011).

In 1969, the FAO Panel of Experts on Forest Genetic Resources prioritized the utilization and conservation to Gmelina arborea (FAO 1969). This just mirrored that many tree planters considered gmelina as a very promising species due to its wood and mechanical properties and ease and cheapness of establishment. Large plantations have been established in Asia and the Pacific like Phillippines, and Malaysia, Fiji Islands, Solomon Islands, and Indonesia. Ataguba (2015) found out that the Gmelina's mechanical characteristics include: compression parallel to grain=7.4 MPa; compression perpendicular to grain=2.5 MPa; tensile strength =6.5MPa and shear strength of 1.3 MPa

The coconut palm (*cocos nucifera*) is also one of the amazing trees in all tropical regions almost because 90% of this tree can give many astonishing benefits to human beings (Vogel, 2005). Air-dried outer part of the solid coco-lumber were found as 50% higher compared to its inner part under both conditions (Khairul,2009). The denser grades of coconut wood can be used as structural material while the lower grades are suitable for joinery and interior use. (FAO Forestry Paper, 1985). Bending strength of its lumber is between 16.34 – 109.21 MPa; Bending stiffness (MOE) of 1.982 – 12.705 MPa; compressive srtength of 9.84 – 77.56 MPa and Shear strength (parallel to grain) of 2.1 – 17.37 MPa (Oduor & Githiomi, n.d.).

White Lauan is from the family of angiosperm or scientifically knows as Shorea contorta which typically come from the Philippines. It is mechanical properties include its crushing strength at a mean of 46 Mpa, mean static bending strength of 80 Mpa, and MOE at 12330 Mpa. It is commonly used for interior joinery, furniture components, form works and veneer plywood (CIRAD, 2012).

Related Studies

In this section, the researcher presents related studies which were reviewed in lieu of the present study. Particularly, the researcher extensively read and marked papers about wood properties of furniture material, testing procedures, failure characteristics of wood, different wood joints and joint performances.

Wood Properties, Strength and Testing Procedures

USSDA (1999) explained that there are factors that affect the strength of the wood which are categorized into: material factors, environmental factors and load factors. As explained, as specific gravity increases, strength properties increase because internal stresses are distributed among more molecular material. The environmental influences can increase the variability of the wood material and, thus, increase the variability of the mechanical properties. Hygroscopic material, such as woods gain or lose moisture to equilibrate with its immediate environment. Winandy (1955) and USSDA (1999) explained that the load being applied to a certain period of time either shorter or longer can cause certain failure. Further, repeated loadings induce fatigue failures often which is a measure of a

material's ability to resist repeating, vibrating, or fluctuating loads without failure. This failure often result from stress levels far lower than those required to cause static failure (Winandy & Rowell, 2005).

Material's resistance to imposed loads relates to its mechanical properties. These include: measures of resistance to deformations and distortions (elastic properties); measures of failure-related (strength) properties, and measures of other performance-related issues. Mechanical properties have two concepts: the stress and the strain. Three types of primary stress that exist in wood: (1) tensile stress-which pulls or elongates an object; (2) compressive stress-which pushes or compresses an object and (3) shear stress - causes two contiguous segments (i.e., internal planes) of a body to rotate (i.e., slide) within the object. Secondary stress includes bending stress - which is a combination of all three of the primary stresses and causes rotational distortion or flexure in an object (Green et.al, 1999; Winandy & Rowell, 2018) These properties are tested as shown in the figure below:

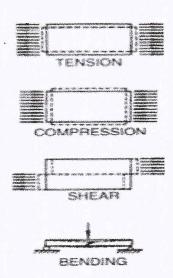


Figure 2. Mechanical Properties of Wood

Source: Winandy & Rowell (2018)

Strain is another important concept of mechanical properties wood. It is the measure of a material's ability to deform—that is, elongate, compress, or rotate—while under stress. Elastic theory asserts that there is such ability of the materials to be deformed due to stress to its ability to regain its original dimensions as removed. Further, Elasticity is the ability of a material to completely regain its original dimensions when the stress is removed which is the opposite quality of viscosity or plasticity. The deformation on immediate unloading, tend to be recoverable that explains that wood is not ideally elastic; rather considered a viscoelastic material (Winandy & Rowell, 2018)

There are two main elastic moduli. These are modulus of elasticity that describes the relationship of load (stress) to axial deformation (strain), and modulus of rigidity or shear modulus, that describes the internal distribution of shearing stress to shear strain or, more precisely, angular (i.e., rotational) displacement within a material (Winandy & Rowell, 2018).

Failure Characteristics of Wood Furniture

Failure characteristics of wood furniture fall into two groups either due to design or due to manufacturing. Failure of woods due to design include furniture parts that are too small and incorrectly configured joints caused by incorrect measurement, cutting, assembling and fitting while wrong wood species, parts or

moisture content are some of the common failure characteristics of wood furniture due to manufacturing (Huber &Eckelman,1999;Boadu &Boasiako,2017).

Jivkov and Marinova (2006) and Dos Santos et al. (2015) explained that the strength properties of the timber could be the major factor underlying the failure of the wood members and their joints. Likos et al. (2012) mentioned that the dimensions and designs selected for construction of joint parts affect their strength. Similarly, Lau (1991) noted that joints failed depending on the geometry of the connection, which could give an indication of their strength.

Compression failures are characterized as crumpling or buckling of cells which usually appear as white lines or may even be invisible to the naked eye.

This failures indicates fiber breakage on end grain and tension wood fibre.

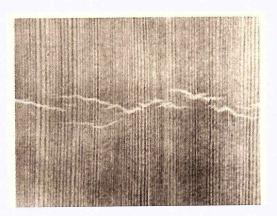


Figure 3.1. Crumpling or buckling of cells



Figure 3.2. Fiber breakage on end grain

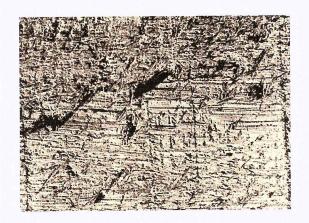


Fig. 3.3. Tension wood fibre

Source: Green et al.(1999), Forest Wood Handbook

Different Wood Joints

Wooden furniture is preferred to over plastic and metal counterparts due to ecological and aesthetic properties of wood (Abdolzadeh et al. 2015). The strength of its joints and members are the main cause of its rigidity (Aicher et al.

2013). Most manufacturer choose joint depending on intended use of the product and the level of strength required (Zhang and Eckelman, 1993).

The City Guide Textbook on Carpentry and Joinery identified the following common wood joints.

Butt joint. Butt joints are the simplest joint, where one piece fasten against another and is fixed with nails or screws. These joints are usually used for constructing study work. The nails or screws used to fix the joints can be 'dovetailed' (skewed) in order to increase the strength of the joint.

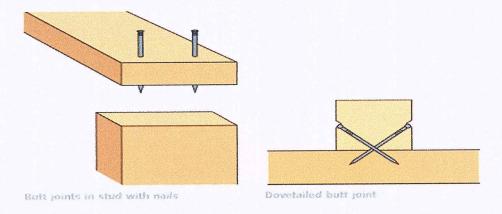


Figure 4.1. Butt Joints

Roofing joints. Roof rafters have these joints. The 'plumb cuts' are the vertical cuts while 'seat cuts' are the horizontal cuts while the 'birdsmouth cut' is the plumb and seat cut together at the bottom of the rafter..

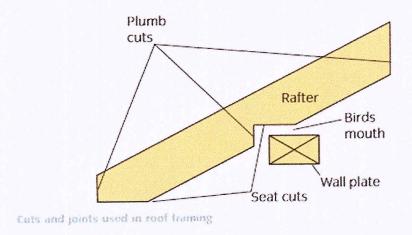


Figure 4.2. Roofing Joints

Halving joint. This joint consist of half two pieces of timber joined together and removed as flush with one another. Commonly, this joint is used in lengthways or simple frames.

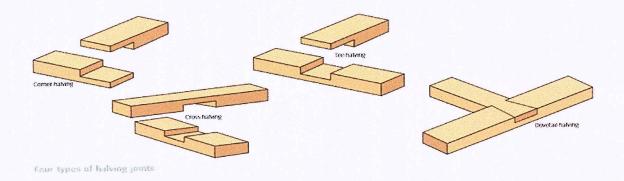


Figure 4.3 Halving Joint

Bridle joint. This is a simple framing joint which the timber is divided into three equal parts in thickness with the centre piece is removed while the two outside joints are removed on the other. This joints is found to be stronger that a halving joint and also be secured using nails, screws or adhesives.

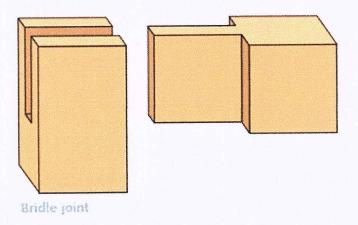
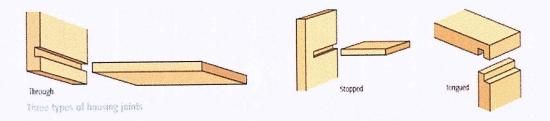


Figure 4.4. Bridle Joint

Housing joint. This joint is commonly used for wide materials to suit varying circumstance like stopped and tounged (barefaced). often, these are intended for door lining/shelving or stair construction which can also be secured with nails, screws and adhesives.



Mitre joint. This joint is used to connect moulder finishes such as skirting or architraves which can be fixed in a place with nails or pins or adhesive. Figure

Figure 4.5. Housing Joints

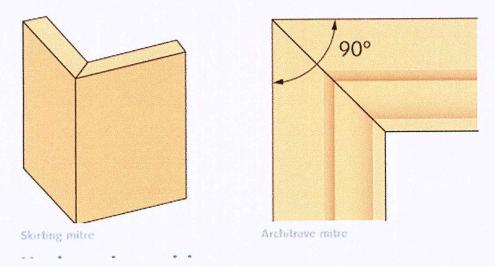


Figure 4.6. Mitre Joints

Mortise and tenon joint. This is the most common joint since it is a very strong and available in many variations. The mortise is a slot, known as the female part, and the tenon known as the male part fits in to a slot. Mostly used in window and door frame, door and sash construction which can be secured

using wedges, adhesive and sometimes screws nails or dowels if used iconstruction of frames.

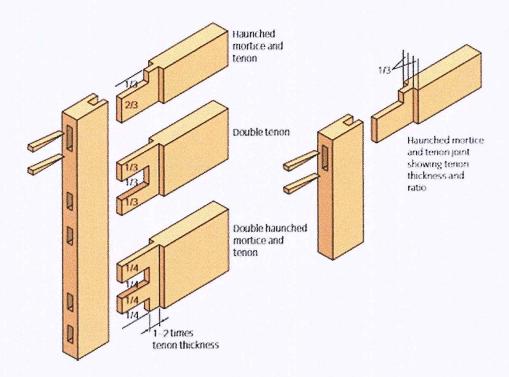


Figure 4.7. Mortise and Tenon joints

Dovetail joint. Traditionally, this is used in the construction of drawers. this joints are connected using adhesives alone. The pitch resists the joint being pulled apart under load. Softwood uses 1:6 angle while 1:8 for hardwoods while some uses an average of 1:7.

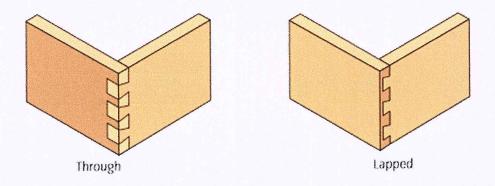


Figure 4.8. Dovetail Joints

Lengthening joint. Lengthening joints can be either structural or non-structural. A heading joint is the most common non-structural lengthening joint like a floor or skirting board as jointed in its length which can be simply square or 'splayed'. Further, scarf joint is also a type of non-structural joint for timber and veneers and used in ridge board while structural lengthening joint is often required where load bearing components require jointing such as a ridge board or purlin used in roof construction.

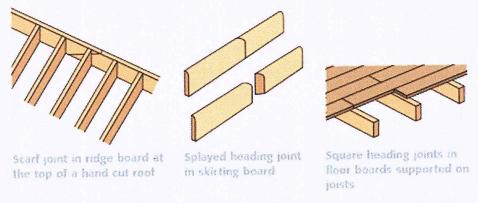


Figure 4.9. Lengthening Joints

Edge joint. This joint is used to make timber boards wider which can be 'rubbed', tongued, biscuited or doweled to increase strength to increase the interconnection of the joint.

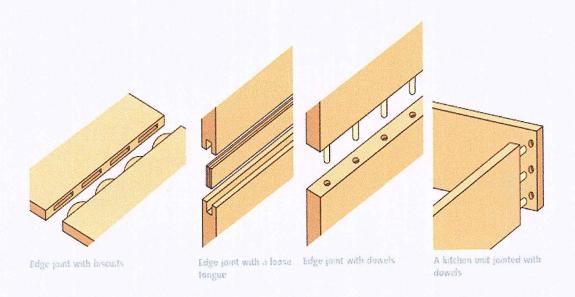


Figure 4.10. Edge Joints

Performance of Dovetail Joints and Mortise and Tenon Wood Joints

The strength of the joints in furniture/woodworking depends on the design of the parts and appropriateness of the timber for the construction (Boadu &Boasiako,2017). Joints that greatly resist bending, compression and tensile forces are the most preferred (Smardzewski, 2015).

Several studies have compared the strength of dovetail joints and mortise and tenon joints in furniture and found out that dovetail joints have great resistance to tension from bending forces and could offer an alternative to mortise-

tenon.Boadu &Boasiako ,2017; Zhang & Eckelman (1993) and Hoadley (2000). This was because dovetail represents quality and artisanship in furniture and timber building construction due to its admirable grain-to-grain surface connection that overcomes warping. The pins and tails interlock to create a stronger natural mechanical bond with better ability to resist bending forces than mortise-tenon (Edwards, 2012).

It was observed in an experiment on withdrawal strengths of dovetail, mortise-tenon and dowel joints that dovetail had greater strength than mortise-tenon joints (Su and Wang,2007). Further, the performance of dovetail halving joint in leg-and-rail construction constructed with dovetail joints were 70% stronger than those with mortise-tenon joint (Asomani,2009). However, it was noted that the use of dovetail for joining legs, slats and stretchers to rails of chairs was not prominent among manufacturers compared to mortise-tenon since dovetail joints require greater level of care and practice in their construction (Fairham, 2007; Tankut & Tankut,2005).

Tankut and Tankut (2005) stressed that mortise-tenon is the most used joint for manufacturing working chairs due to their strength against twisting and the ease of assembly. However, joints break down with time when chairs are subjected to bending stresses that stretch wood fibres during the sitting process (Eckelman & Haviarova, 2006). Experimental studies have found out that rectangular end mortise and tenons are stronger than both round end mortise and tenons and rectangular end tenons fitting into round end mortise joints. Joint

geometry shows a significant effect on the strength of those particular joints which is characterized that as tenon width and length were increased, the strength of the joint was correspondingly improved (Erdil et al., 2005; Haviarova et al., 2013; Fine Woodworking 2004).

Some finding also show that there was a greater strength for joints made from 60 mm wide and 45 mm long tenon (393 N m) than those from 30 mm wide and 20 mm long (125 N m) (Kasal et al., 2013) which finding was similar with Erdil et al. (2005) that there is an increase in joint strength when tenon length and width were increased from 12.7 to 50.8 mm and 12.7 to 76.2 mm, respectively. Added by Hajdarević & Martinović (2014), longer and thicker tenons are not easily pushed out of the mortise when stressed making stronger joints than shorter and thinner tenons.

Ratnasingam et al. (2010) stressed that the decision to use a particular timber species and a corresponding joint design for furniture production must be based on experimental results of the performance of the wood-joint design combination. However, the reviewed literature and studies showed no enough studies conducted regarding GMELINA, COCO and WHITE LAUAN wood properties if joints are constructed through dovetail and mortise and tenon joinery methods that prompted the researcher to explore by conducting an experiment regarding the performance of wood joints.

Chapter 3

METHODOLOGY

This chapter discusses the research design, instrumentation, sampling procedure, data gathering procedure as well as statistical tools and treatment that will be used to analyze and interpret the data gathered.

Research Design

This study employed an experimental research design where the variables were carefully tested and/or manipulated.

Instrumentation

The researcher used *ASTM D4761* or the Standard Test Methods for Mechanical Properties of Lumber and Wood-Based Structural Materials in testing the performance of Gmelina, Coconut and White Lauan softwoods. The testing machine used in the experiment was the Computer Display Hydraulic Control Universal Testing Machine (100 kN Cap.), JINAN, Model: WEW-100D for Compression, Tension and Flexural Tests and Shear Test Set-up which were conducted at Northwest Samar State University (NWSSU) Laboratory in Calbayog City, Western Samar with the help of a competent personnel in-charge.

Other tools used in the conduct of the impact testing were the pull-push rule measurements, wooden flat surface, wooden sticks for balancing to a high level, claw hammer for installation and forming positions.

Sampling Procedure

Lumber are sampled by its quality and characteristics and known to be a softwood type. Lumber was prepared though following steps:

- 1. Planed the lumber into desired size
- 2. Measure the lumber to its required length
- 3. Cut it into pieces
- 4. Labeling samples

For the material used in Impact Test and Shear test

- 1. Measure both end to prepare the tenon tonque or dovetail tonque
- 2. Cut and shape to fit it into the mortise hole or dovetail hole
- 3. Assemble and fix it correctly
- 4. Labeling samples

Below are the samples tested according to wood specie and test performed.



Figure 5.1. Sample of Wood Specimen for White Lauan Specimen 1



Figure 5.2. Sample of Wood Specimen for Compression Parallel to Grain



Figure 5.3. Sample of Wood Specimen for Compression Perpendicular to Grain



Figure 5.4. Sample of Wood Specimen for Flexural/Tension Test



Figure 5.5. Sample of Wood Specimen for Shearing Test



Figure 5.6. Sample of Wood Specimen for Impact Test

Data Gathering Procedure

Data gathered in this study include 4 sets of tests: compression, flexural/tensile, shear and impact. Compression, flexural/tensile, shear testings were done following the ASTM D4761 or the Standard Test Methods for Mechanical Properties of Lumber and Wood-Based Structural Materials using Computer Display Hydraulic Control Universal Testing Machine.

Compression Test. The three groups of lumbers were tested in 3 trials following ASTM D4761.

Flexure Test/Bend Test. The three groups of lumbers were tested following ASTM D4761.

Shear Test. The three groups of lumbers made of triangular dovetail joints and rectangular mortise and tenon joints were tested following ASTM D4761.

Impact Test. The test performed was a modified test derived from ASTM D4761. the following figures below shows the detailed steps of testing.

Figure 6. Schematic Diagram Showing the Impact Test Process

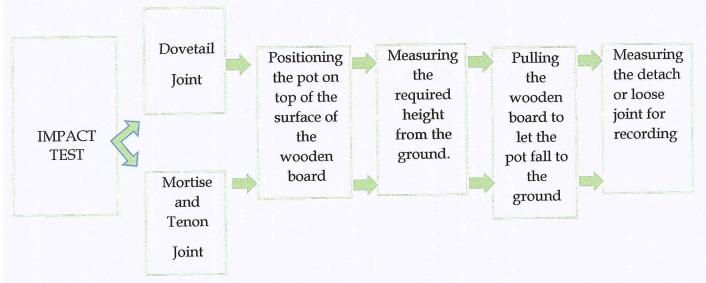


Figure 7 Construction of Joints

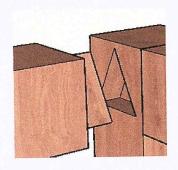


Figure 7.1. Dovetail Joint

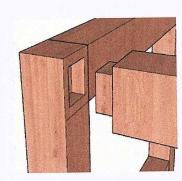


Figure 7.2. Mortise and Tenon Joint

3. Positioning the pot on top surface

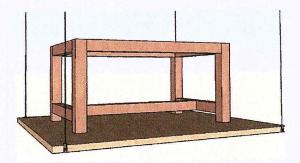


Figure 7.3. Positioning the pot on top surface

3. Measure the required heigth from the ground

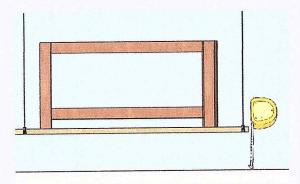


Figure 7.4. Measure the required height from the ground

4. Pull the wooden surface to let the pot fall to the ground.

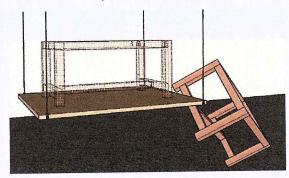


Figure 7.5. Pull the wooden surface to let the pot fall to the ground

5. Measure the detach or loose joint for recording.

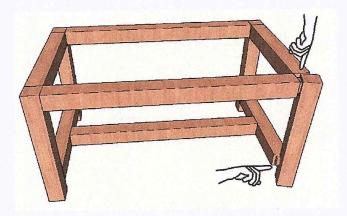


Figure 7.6. Measure the detach or loose joint for recording

Data Analysis

The data were proposed by the UTM operator based on the computerized result of the UTM Machine for all the wood specimens tested. In determining the performance of wood specimen in terms of compression, flexure/tension and shear test, data were utilized through the measures of central tendency and the spread of data per wood specie. Using ANOVA, the differences of the performance of the wood specimens were tested considering the wood specie, dimension and type of joints. All statistical tests were done using SPSS.

Chapter 4

PRESENTATION, ANALYSIS AND INTERPRETATION OF DATA

This chapter presents the data collected, analyzed and interpreted. Specifically, this presents the performance of softwood samples in terms of compression tests and tensile/bending tests and wood joints in terms of shearing and impact tests.

Table 1

Compression Test Results of Softwood in terms of Dimension and Wood Specie

Table 1.1

Compression Test Results of Wood Samples Parallel to Grain

GMELINA	Width 1 (mm)	Width 2 (mm)	Area	Indicated Maximum Load(kN)	Compressive Strength (MPa)
GL PARS1	43	50	2150	59.1	27.5
GL PARS2	44	50	2200	58.2	26.5
GL PARS 3	40	51	2040	59.4	29.1
Average	42	50	2130	58.9	27.7
COCO					
CO PARS1	41	51	2091	52.1	24.9
CO PARS2	47	43	2021	45.7	22.6
CO PARS3	43	52	2236	34.6	15.5
Average	44	49	2116	44.1	21.0
WHITE					
LAUAN					
WL PARS1	43	52	2236	37.5	16.8
WL PARS2	43	52	2236	37.5	16.8
WL PARS3	41	51	2091	52.5	25.1
Average	42.3	51.7	2188	42.5	19.6

The table 1.1 shows that GMELINA with an average compressive strength (MPa) =27.7 was found stronger than COCO and WHITE LAUAN woods with an average compressive strength (MPa) = 21.0 and 19.6 respectively.

Further, the compressive strength (MPa) of the wood samples from GMELINA, COCO and WHITE LAUAN were directly relative to their Indicated Maximum Load (kN) from sample 1-3 and among these, GMELINA was still found to have the highest average Indicated Maximum Load (kN) of 58.9 followed by COCO and WHITE LAUAN with 44.1 and 42.5 respectively. This implies that GMELINA is found to be a strong and durable wood material that carpenters must consider in furniture-making and woodworking among the identified woods as clearly depicted in Figure 7. The experiment result was higher compared to the findings of Ataguba (2015) with compression parallel to grain=7.4 MPa. These findings were evident during the experiment where it has been noted that a compressive stress appeared in GMELINA wood sample caused by the large cracks along the grain while COCO wood sample has a fractured fiber hair with radial cracks and a horizontal hair-like type cracks on its fibred end-grain. WHITE LAUAN wood sample has been deformed from its original shape with a minor crack from the compressive stress in the grain. (Please see Appendix B-1 &2 Preliminary and Final Observation in Compression Test Parallel to Grain).

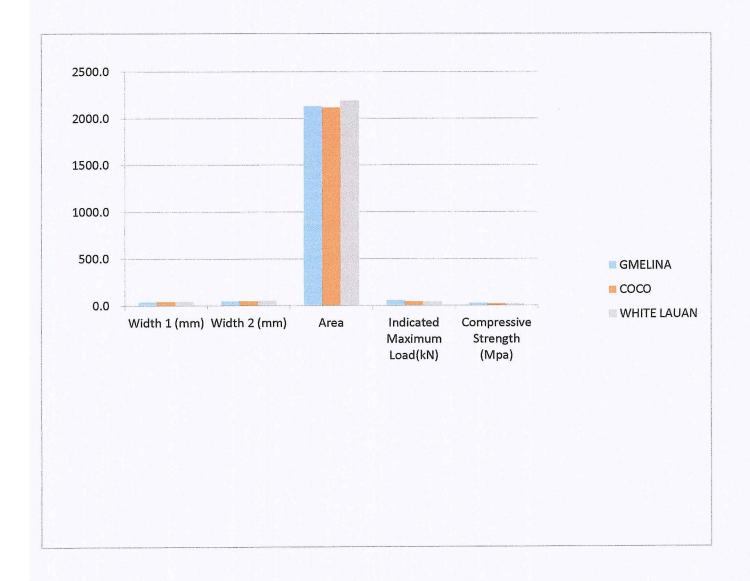


Figure 8. Compression Strength Parallel to Grain

Table 1.2

Compression Test Results of Wood Samples Perpendicular to Grain

GMELINA	Width 1 (mm)	Width 2 (mm)	Area	Indicated Maximum Load(kN)	Compressive Strength (MPa)
GL PERS1	46	52	2392	18	7.5
GL PERS2	46	51	2346	9.6	4.1
GL PERS3	46	51.5	2369	13.8	21.3
Average	46	51.5	2369	13.8	10.97
COCO					
CO PERS1	50	4.9	2450	8.9	36.3
CO PERS2	42	4.9	2058	12.3	6
CO PERS3	46	4.9	2254	10.6	21.2
Average	46	4.9	2254	10.6	21.2
WHITE LAUAN					
WL PERS1	45	50	2250	46.1	20.5
WL PERS2	45	50	2250	40.9	18.2
WL PERS3	45	50	2250	43.5	4.5
Average	45	50	2250	43.5	14.4

The table 1.2 shows that COCO with an average compressive strength (MPa) of 21.2 was found higher than WHITE LAUAN and GMELINA woods with an average compressive strength (MPa) = 14.4 and 10.97 respectively as shown in Figure 8. Further, it was observed that there was a variability of the compressive strength perpendicular to grain on the loading direction of the 3 trials per wood specie and was found to be lower than the compressive strength parallel to grain. This was due to the fact that the resistance of wood perpendicular to the grain is simply a matter of the resistance offered by the wood elements to being crushed or flattened given in the literature. This result had shown similarities with Oduor

& Githiomi, (n.d.) which compressive strength falls from the range of 9.84 – 77.56 MPa of COCO lumbers.

These findings were evident since it has been observed that GMELINA and WHITE LAUAN wood samples produced a linear fracture across the grain caused by the high compressive stress while COCO wood sample has an earth wood failure and small cracks along the grains caused by the high compressive stress. (Please see Appendix C-1&2 Preliminary and Final Observation in Compression Test Perpendicular to Grain).

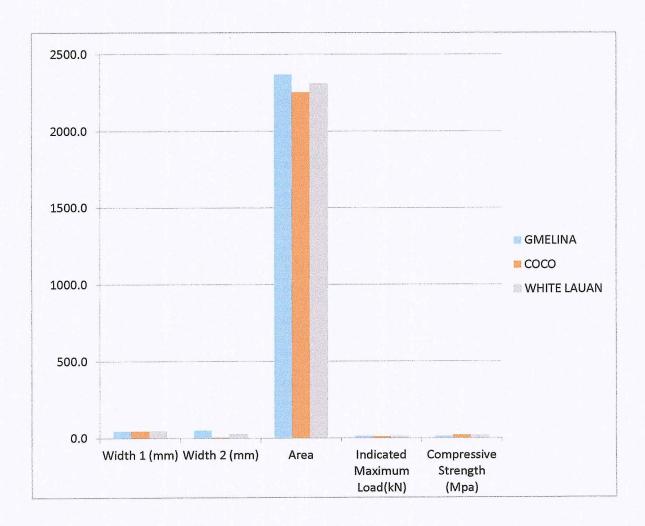


Figure 9. Compression Strength Perpendicular to Grain

Table 2

Bending and Tension Test Results on Wood Samples Parallel to Grain

GMELINA	Width 1 (mm)	Width 2 (mm)	Area	Indicated Maximum Load(kN)	Compressive Strength (MPa)	
GL BTS1	46	51	0.23	11.3	32.7	
GL BTS2	47	51	0.23	14.895	42	
GL BTS3	47	51	0.24	9	26.5	
Average	46.7	51.0	0.2	11.7	33.7	
COCO						
CO BTS1	40	45	0.23	1.7	7.4	
CO BTS2	40	45	0.23	1.7	7.4	
CO BTS3	46	52	0.24	5.2	15.1	
Average	42	47.3	0.2	2.9	10.0	
WHITE						
LAUAN						
WL BTS1	46	51	0.24	10.3	31	
WL BTS2	46	51	0.24	10.3	31	
WL BTS3	46	51	0.24	10.3	31	
Average	46	51	0.24	10.3	31	

The table 2 shows that GMELINA with an average bending/tension strength (MPa) of 33.7 was found higher than WHITE LAUAN and COCO woods with an average bending/tension strength (MPa) = 31 and 10 respectively.

Further, as shown in the data, the bending/tension strength (MPa) of the wood samples from GMELINA, COCO and WHITE LAUAN were directly relative to the Indicated Maximum Load (kN) from Trials samples 1-3 and among these, GMELINA was still found to have the highest average Indicated Maximum Load (kN) of 11.7 followed by WHITE LAUAN and COCO with 10.3 and 2.9 respectively. This implies that GMELINA is found to be a strong and durable wood material that carpenters must consider in furniture-making and

woodworking using softwoods. This finding are within the range of strength reported in the previous studies by Agatuba (2015), Oduor & Githiomi, (n.d.) and CIRAD, (2012). This is clearly depicted in Figure 9.

These finding were evident during the bending/tensile testing, where it was observed that there was a tension failure under bending in GMELINA wood samples similar with COCO wood samples but with a quite long-fibred tension than GMELINA wood sample. It was also noticed that WHITE LAUAN has a short-fibred tension failure parallel to grain. (Please see Appendix D-1&2-Preliminary and Final Observation in Bending/Tension Test Parallel to Grain).

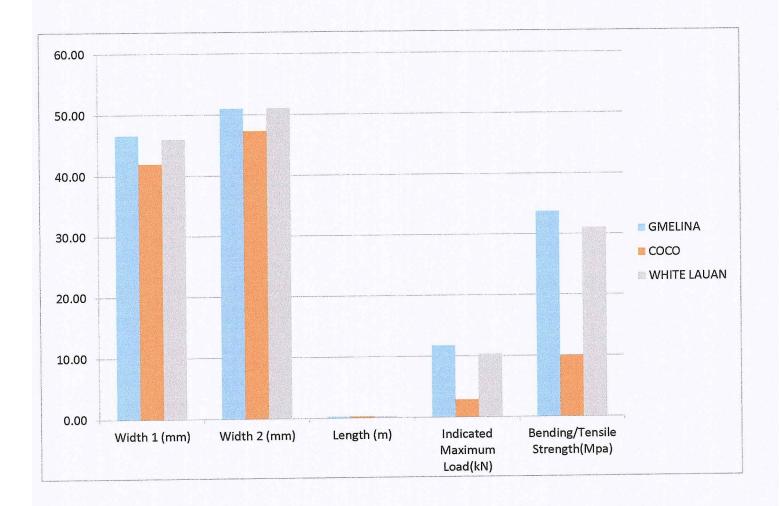


Figure 10. Bending and Tensile Strength Parallel to Grain

Table 3

Shear Test Results of Dovetail Joints Perpendicular to Grain

GMELINA Dovetail Joint	Area (mm²)	Indicated Maximum Load(kN)	Shear Strength (MPa)	
GL DTS1	357	10.9	30.4	
GL DTS2	748.38	9.8	13.1	
Average	552.69	10.35	21.75	
COCO Dovetail Joint				
CO DTS1	402	1	2.6	
CO DT S2	410	8.1	19.8	
Average	406	4.55	11.2	
WHITE LAUAN Dovetail				
Joint				
WL DTS1	548.38	2.7	4.9	
WL DTS2	320	9.7	30.3	
Average	434.19	6.2	17.6	

The Table 3 presents the Shear Test Results of Dovetail Joints Perpendicular to Grain.

The data reveals that GMELINA dovetail joints with an average area (A=552.69 mm²) and an average yield to an indicated maximum load of (kN)=10.35 has an average shear strength of (MPa)=21.75 has a greater strength than WHITE LAUAN and COCO dovetail joints with an average MPa of 17.6 and 11.2 respectively.

Further, as shown in the data, the shear strength (MPa) of dovetail joints of the wood samples from GMELINA, COCO and WHITE LAUAN were directly relative to the Indicated Maximum Load (kN) from Trials 1 to 3 and among these, GMELINA was still found to have the highest average Indicated Maximum Load

(kN) of 10.35 followed by WHITE LAUAN and COCO with 6.2 and 4.55 respectively.

This implies that GMELINA is found to be a strong and durable wood material among the wood species used in the study which carpenters must consider in furniture-making and woodworking using softwoods. This is clearly depicted in Figure 10.

Further, this implies that GMELINA and WHITE LAUAN Dovetail Joints with smaller area have greater shear strength than those with bigger area of wood samples. This finding was in opposite with COCO wood sample which has resulted to an 85% increase in shear strength in COCO sample 2 having a very minimal increased area which led to an increase in the maximum load of almost 90%. This finding are within the range of strength reported in the previous studies by Agatuba (2015), Oduor & Githiomi, (n.d.) and CIRAD, (2012).

These findings were noted during the observation that GMELINA dovetail joint has a shear tension failure causing the tenon to slide longitudinally on beam and broke the dovetail joints. COCO dovetail joints were detached on hole and cracked continually on longitudinal surface. Similar with COCO dovetail joints, WHITE LAUAN dovetails pin joints were also pulled-out on hole and produced a small horizontal hair-type cracks. (Please see Appendix E-1&2 Preliminary and Final Observation in Shear Test Perpendicular to Grain

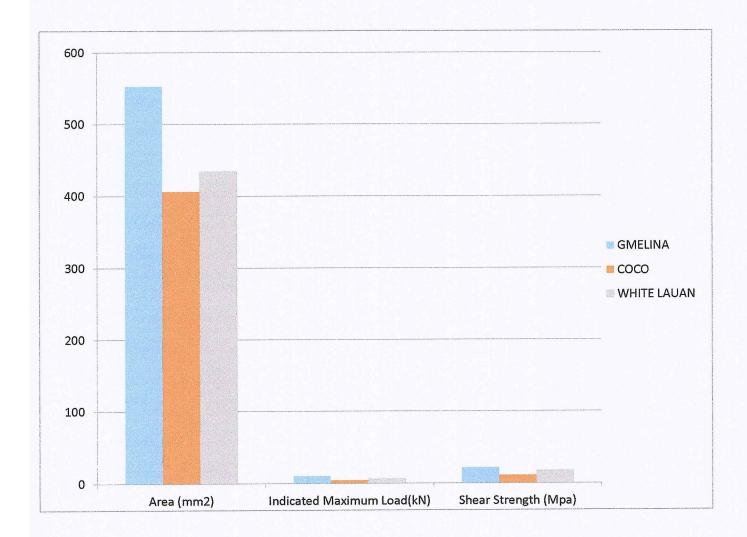


Figure 11. Shear Strength of Dovetail Joints

Table 4

Shear Test Results of Mortise and Tenon Joints Perpendicular to Grain

GMELINA Mortise &Tenon Joint	Area (mm²)	Indicated Maximum Load(kN)	Shear Strength (MPa)	
GL MTS1	1147	8.6	7.5	
GL MTS2	899.04	7.3	8.1	
Average	1023.02	7.95	7.8	
COCO Mortise and				
Tenon Joint				
CO MTS1	1150	2.5	2.1	
CO MT S2	1148	8.7	7.6	
Average	1149	5.6	4.85	
WHITE LAUAN				
Mortise and Joint				
WL MTS1	899.04	3.1	3.5	
WL MTS2	1147	5.3	4.6	
Average	1023.02	4.2	4.05	

The table 4 shows that GMELINA mortise and tenon joints with an average area (A=1023 mm²) yield to an indicated maximum load of (kN)=7.95 has an average shear strength (MPa) of 7.8 compared to COCO with an area (A=1149 mm²) yield to an indicated maximum load of (kN)=5.6 has an average shear strength of (MPa)=4..85 while WHITE LAUAN with an average area (A=1023 mm²) yield to an indicated maximum load of (kN)=4.2 has an average shear strength of (MPa)=4.05 as shown in Figure 11. This finding contribute to the body of knowledge that Gmelina has relatively higher strength than COCO and WHITE LAUAN constructed using the mortise and tenon joints.

These findings are seen during the shearing test where GMELINA mortise and tenon joints failed and produced cracks at the end of the beam causing to a fractured tenon joint. COCO mortise and tenon joints also failed in the shear

test, however, unlike GMELINA joint, the COCO tenon joints were pulled-out from the mortise tenon hole and cracked into a longitudinal surface. WHITE LAUAN mortise and tenon joints also have the shear tension failure causing the tenon joint continually to a longitudinal surface. (Please see Appendix E-1&2 Preliminary and Final Observation in Shear Test Perpendicular to Grain)

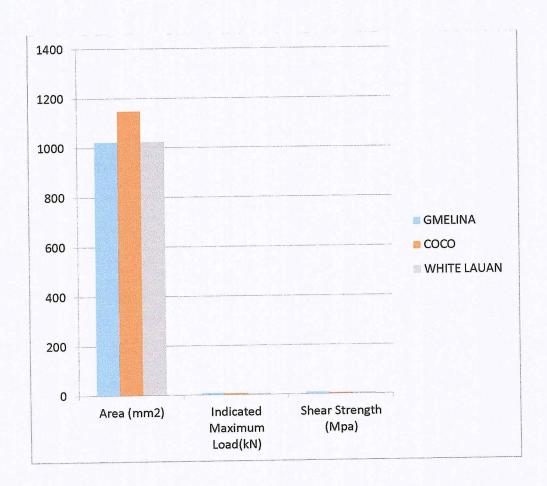


Figure 12. Shear Strength of Mortise and Tenon Joints

Table 5

Comparative Analysis on Impact Testing Results of Dovetail Joints and Mortise and Tenon Joints on Wood Projects

JOINTS	GME	LINA	CO	СО	WHITE	LAUAN			
	DOVETAIL JOINTS								
TEST	Dragged (mm)	detached	dragged (mm)	detached	dragged (mm)	detached			
PRELIM	43mm	6 joints	60mm	6 joints	46mm	0			
FINAL	67mm	5 joints	43mm	0	58mm	1 joint			
Total	110 mm	11 joints	103 mm	6 joints	104 mm	1 joint			
		MORTISE	AND TENO	ON JOINTS					
PRELIM	49mm	3 joints	44mm	6 joints	24mm	0			
FINAL	52mm	4 joint	51mm	9 joint	40mm	0			
Total	101 mm	7 joints	95 mm	15 joints	64 mm	0			

The table shows that among the two joint, dovetail joints made of Gmelina got the highest recorded dragged position upon impact test from several heights than mortise and tenon joints of the different wood samples while Coco mortise and tenon joints got the highest recorded detached joints among other wood species.

On an average, the data shows that mortise and tenon joints perform better than dovetail joints among GMELINA, COCO and WHITE LAUAN.

Analysis of Variance (ANOVA) on the Compression Strength of Softwood in terms of Dimension and Wood Specie

Table 6

Table 6.1

Analysis of Variance (ANOVA) on the Compression Strength Parallel to Grain in terms of Dimension and Wood Specie

Dependent Variable: Compression Strength (MPa)

Test	df	F	p-value	Interpretation
Overall Model	6	26.192	.037	Significant
Wood	2	31.921	.030	Significant
Area	2	27.752	.035	Significant

p= <.05 = Significant p= ≥.05 = Not significant

The data show that the test of compression parallel to grain in the overall ANOVA model df=6(F, 26.192) p=.037 made the strength of wood samples significantly different with underlying parameters. This implies that there was a significant difference between the compression strengths parallel to grain of softwoods as to its dimension and wood specie which rejected the null hypothesis of the study at .05 level of significance.

Particularly, the wood species GMELINA and COCO were found statistically different at p=.042 which implies that the average strength of GMELINA was significantly greater than COCO and shall be considered an option for furniture materials.

Table 6.2

Analysis of Variance (ANOVA) on the Compression Strength Perpendicular to Grain in terms of Dimension and Wood Specie

Dependent Variable: Compression Strength (MPa)

F		<u> </u>		
Test	df	F	p-value	Interpretation
Overall Model	4	1.967	.264	Not significant
Wood	2	3.270	.144	Not significant
Area	2	2.909	.166	Not significant

p= <.05 = Significant p= ≥.05 = Not significant

The data show that the test of compression perpendicular to grain in the overall ANOVA model df=4(F, 1.967) p=.264 made the compression strength of softwoods show no difference with underlying parameters. Further, there was no significant difference between the compression strengths perpendicular to grain of softwoods as to its dimension and the identified wood specie. This accepted the null hypothesis of the study. This finding contributes to the body of literature that GMELINA, COCO and WHITE LAUAN have no significant difference as to its compression strength perpendicular to grain.

Table 7

Analysis of Variance (ANOVA) on the Bending/Tensile Strength Parallel to Grain in terms of Dimension and Wood Specie

Dependent Variable: Bending/Tensile Strength Parallel to Grain (MPa)

Test	df	F	p-value	Interpretation
Overall Model	4	.999	.628	Not significant
Wood	2	.089	.921	Not significant
Area	2	1.596	.488	Not significant

p = <.05 = Significantp = <.05 = Not significant

The data show that bending/tensile strength perpendicular to grain in the overall ANOVA model df=4(F=.999) p=.628 showed no significant difference with underlying parameters. This implies that bending/tensile strength parallel to grain of softwoods were not different as to its dimension and wood specie. This finding accepted the null hypothesis of the study at .05 level of significance. This implies that among the tested wood samples, wood specie and area/dimension did not make any differences as to the bending/tensile strength of the wood of GMELINA, COCO and WHITE LAUAN. This finding contributes to the body of literature that GMELINA, COCO and WHITE LAUAN have no significant difference in terms of its bending or tensile strength parallel to grain.

Table 8

Analysis of Variance (ANOVA) on the Shear Strength of Dovetail Joints and Mortise and Tenon Joints in terms of Dimension and Wood Specie

Table 8.1
Analysis of Variance (ANOVA) on the Shear Test Performance of Dovetail
Joints and Mortise and Tenon Joints in terms of Dimension

Dependent Variable: Shear Strength

Test	df	F	p-value	Interpretation
Overall Model	2	2.400	.146	Not significant
Joints	1	2.469	.151	Not significant
Area	1	.203	.663	Not significant
Joints vs. Area	0	0	0	No interaction

p= <.05 = Significant p= >.05 = Not significant

The data show that the shear strength perpendicular to grain of the dovetail joints and mortise and tenon joints in the overall ANOVA model df = 2(F, 2.400) p=.146 showed no significant difference with underlying parameters. This implies that the shear strength perpendicular to grain were not different as to its dimension and wood specie. This finding accepted the null hypothesis of the study at .05 level of significance. Further, no relative reactions or significant evidence shown in the experiment that the 3 types of wood with its specific dimensions will result to a greater strength of mortise and tenon joints than dovetail joints or the reverse. Therefore, both joints are still effective in any construction of wooden projects like those in the furniture making industry. Thus, this finding adheres in the literature that joinery methods are useful provided that the standards prescribed in making any wooden projects like

furniture are specifically designed and joints are carefully chosen which will make the construction more effective (Likos et al., 2012). However, this finding caught exemption of the existing literature on the interaction of joints and its dimension.

Table 8.2

Analysis of Variance (ANOVA) on the Mean Shear Test Performance of Dovetail Joints and Mortise and Tenon Joints in terms of Wood Specie

Dependent Variable: Shear Strength

Test	Df	F	p-value	Interpretation
Overall Model	5	.963	.506	Not significant
Joints	1	3.360	.106	Not significant
Wood	2	.434	.677	Not significant
Joints vs. Wood	2	.173	.846	Not significant

p = <.05 = Significant $p = \ge.05 = Not significant$

The data show that the shear strength perpendicular to grain in the overall ANOVA model d5=4(F=.963) p=.506 showed no significant difference with underlying parameters. The shear strength perpendicular to grain of softwoods were not different as to its dimension and wood specie. This finding accepted the null hypothesis of the study at .05 level of significance. This finding was in exemption of the existing literature that dovetail joints are stronger than mortise and tenon joints (Boadu &Boasiako ,2017; Zhang & Eckelman ,1993 and Hoadley ,2000; Su and Wang,2007).

Table 9

Analysis of Variance between the Impact Test Performance of the Dovetail

Joints and Mortise and Tenon Joints

Model	Sum of Squares	df	Mean Square	F	Sig.
Regression	82.738	3	27.579	1.949	.142
Residual	452.900	32	14.153		
Total	535.639	35	41.732		

a. Predictors: (Constant), height, wood, joint

p = <.05 = Significant

 $p= \ge .05 = Not significant$

The Table 7.2 presents the Test of Difference between the Impact Test Performance of the Dovetail Joints and Mortise and Tenon Joints

The data shows that the strength of dovetail joints and mortise and tenon joints were not significantly different with p=.142>@=.05 with the predictors: height, type of wood and type of joint.

This implies that both joinery methods were capable to absorb shocks that cause stresses beyond the proportional limit of the joints considering the increased heights and the type of wood used which accepted the null hypothesis of the study.

b. Dependent Variable: maximum change (mm)

Chapter 5

SUMMARY OF FINDINGS, CONCLUSIONS AND RECOMMENDATIONS

Summary of Findings

The findings show that GMELINA with an average compressive strength (MPa) =27.7 was found stronger than COCO and WHITE LAUAN woods with an average compressive strength (MPa) = 21.0 and 19.6 respectively. Further, the compressive strength (MPa) of the wood samples were directly relative to their Indicated Maximum Load (kN). During the experiment where it has been noted that a compressive stress appeared in GMELINA wood sample caused by the large cracks along the grain while COCO wood sample has a fractured fiber hair with radial cracks and a horizontal hair-like type cracks on its fibred end-grain. WHITE LAUAN wood sample has been deformed from its original shape with a minor crack from the compressive stress in the grain.

On compression perpendicular to grain, COCO with an average compressive strength (Mpa) of 21.2 was found higher than WHITE LAUAN and GMELINA woods with an average compressive strength (MPa) = 14.4 and 10.97 .GMELINA and WHITE LAUAN wood samples produced a linear fracture across the grain caused by the high compressive stress while COCO wood sample has an earth wood failure and small cracks along the grains caused by the high compressive stress.

On bending/tension strength, GMELINA with an average bending/tension strength (MPa) of 33.7 was found higher than WHITE LAUAN and COCO woods with an average bending/tension strength (MPa) = 31 and 10 respectively which 0were directly relative to the Indicated Maximum Load (kN). A tension failure under bending in GMELINA wood samples similar with COCO wood samples but with a quite long-fibred tension than GMELINA wood sample and WHITE LAUAN has a short-fibred tension failure parallel to grain.

On shear strength, GMELINA dovetail joints has an average shear strength of (MPa)=21.75 with greater strength than WHITE LAUAN and COCO dovetail joints with an average MPa of 17.6 and 11.2 respectively which were directly relative to their indicated maximum loads. GMELINA dovetail joint has a shear tension failure causing the tenon to slide longitudinally on beam and broke the dovetail joints, COCO dovetail joints were detached on hole and cracked continually on longitudinal surface and WHITE LAUAN dovetails pin joints were also pulled-out on hole and produced a small horizontal hair-type cracks.

On mortise and tenon joints, GMELINA with an average shear strength (MPa) of 7.8 compared to COCO has an average shear strength of (MPa)=4..85 while WHITE LAUAN of (MPa)=4.05. GMELINA mortise and tenon joints failed and produced cracks at the end of the beam causing to a fractured tenon joint. COCO mortise and tenon joints also failed in the shear test, however, unlike GMELINA joint, the COCO tenon joints were pulled-out from the mortise tenon hole and cracked into a longitudinal surface. WHITE LAUAN mortise and

tenon joints also have the shear tension failure causing the tenon joint continually to a longitudinal surface.

On impact strength, findings show that dovetail joints made of Gmelina got the highest recorded dragged position upon impact test from several heights than mortise and tenon joints of the different wood samples while Coco mortise and tenon joints got the highest recorded detached joints among other wood species.

On the test of difference on compression parallel to grain, in the overall ANOVA model df=6(F, 26.192) p=.037 made the strength of wood samples significantly different with underlying parameters. Particularly, the wood species GMELINA and COCO were found statistically different at p=.042 which implies that the average strength of GMELINA was significantly greater than COCO and shall be considered an option for furniture materials.

On the test of compression perpendicular to grain, the overall ANOVA model df=4(F, 1.967) p=.264 made the compression strength of softwoods show no difference with underlying parameters. Further, there was no significant difference between the compression strengths perpendicular to grain of softwoods as to its dimension and the identified wood specie

On the test of difference on bending/tensile strength perpendicular to grain, the overall ANOVA model df=4(F=.999) p=.628 showed no significant difference with underlying parameters.

On the test of difference on shear strength perpendicular to grain of the dovetail joints and mortise and tenon joints, the overall ANOVA model

df=2(F,2.400) p=.146 showed no significant difference with underlying parameters. Further, no relative reactions or significant evidence shown in the experiment that the 3 types of wood with its specific dimensions will result to a greater strength of mortise and tenon joints than dovetail joints or the reverse.

On the test of difference of shear strength perpendicular to grain, the overall ANOVA model d5=4(F=.963) p=.506 showed no significant difference with underlying parameters.

On the test of difference on impact strength, dovetail joints and mortise and tenon joints were not significantly different with p=.142>@=.05 with the predictors: height, type of wood and type of joint.

Conclusions

Based on the findings of the study, the following conclusions were drawn:

On the basis of the findings of the study, it is therefore concluded that:

- Gmelina offers greater wood properties in terms of dimensions. However, this does not necessarily considered as a factors of the strength of other wood samples.
- Gmelina offers a greater strength in terms of compression parallel to grain and tensile strength while coco offers a greater compressive strength perpendicular to grain.
- Dovetail joint offer a greater shear strength and low impact strength compared to mortise and tenon joints.

- 4. Mortise and tenon joints offers relatively low shear strength and a greater impact strength compared to dovetail joint.
- 5. Dovetail joints and mortise and tenon joints have insignificant difference in strength under dimensions and species.
- 6. Dovetail joints and mortise and tenon joints have insignificant difference in shear strength and impact strength.

Recommendations

Based on the conclusions of the study, the following is hereby recommended.

- 1. Gmelina shall be given a place in woodworking, but this should not discout other Philippine woods.
- 2. End-users shall explore more on the properties of Coco lumber as a good material in furniture and woodworking activities.
- 3. End-users shall explore techniques in improving the impact strength of dovetail joints.
- 4. End-users shall explore techniques in improving the shear strength of mortise and tenon joints.
- 5. End-users shall explore more on other wood properties as variables in effect to the better performance of wood joints other than dimension and species.

6. End-users shall explore more on the other properties as variables in the performance of both dovetail and mortise and tenon joints in terms of shear and impact strength.

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SUMMARY OF THE LABORATORY STANDARDIZED TESTING RESULTS OF WOODS

	NAME OF TEST	PRE	LIMINARY	TEST	FI	NAL TEST	
		GMELINA	COCO	WHITE LAUAN	GMELINA	COCO	WHITE LAUAN
		Compressive Strength (Mpa)			Compress	ive Strength	(Mpa)
1.	COMPRESSION TEST PARALLEL TO GRAIN	27.5	24.9	16.8	29.1	15.5	25.5
2.	COMPRESSION TEST PERPENDICULAR TO GRAIN	7.5	36.3	20.5	22.5	18.2	4.6
3.	BENDING AND TENSION PARALLEL TO GRAIN	42	7.4	31.0	26.5	15.1	31
4.	SHEAR PERPENDICULAR TO GRAIN(DOUBLE)						
	Dovetail Joint without Nail or Wood Glue	30.4	2.6	4.9	13.1	19.8	30.3
	Mortise and Tenon Joint without Nail or Wood Glue	7.5	2.1	3.5	8.1	7.6	4.6

	Dovetail Joint without nail or glue								
Height from the Ground	GMELINA		cc	сосо		E LAUAN			
	dragged (mm)	detached	dragged (mm)	detached	dragged (mm)	detached			
½ meter	2	none	2	none	5	none			
1 meter	4	none	10	none	6	none			
1½ meter	10	none	13	none	4	none			
2 meter	2	2	14	1	15	none			
2 ½ meter	15	1	10	3	8	none			
3 meter	10	3	11	2	8	none			
	43mm	6 joints	60mm	6 joints	46mm	0			

Height from the Ground	Λ	Aortise and '	Tenon Joint	without Na	l or Wood C	slue
	GMI	ELINA	CC	oco		E LAUAN
	dragged (mm)	detached	dragged (mm)	detached	dragged (mm)	detached
½ meter	0	none	2	none	2	none
1 meter	6	none	6	none	0	none
1½ meter	16	2	5	none	5	none
2 meter	10	none	14	1	4	none
2½ meter	4	none	9	2	5	none
3 meter	13	1	8	3	8	none
	49mm	3 joints	44mm	6 joints	24mm	0
5IMPACT TEST (FINAL)					<u> </u>	
		Do	etail Joint v	vithout nail		
Height from the Ground	GMI	ELINA	CC	ОСО		E LAUAN
	dragged (mm)	detached	dragged (mm)	detached	dragged (mm)	detached
½ meter	10	none	5	none	10	none
1 meter	15	none	6	none	15	none
1½ meter	10	none	4	none	4	none
2 meter	9	1	15	none	3	1
2 ½ meter	9	2	5	none	10	none
3 meter	14	2	8	none	16	none
	67mm	5 joints	43mm	0	58mm	1 joint
		Mortise and	Tenon Join	t without Na	il or Wood	Glue
Height from the Ground	GM	ELINA	C	осо		TE LAUAN
8 7	dragged (mm)	detached	dragged (mm)	detached	dragged (mm)	detached
½ meter	4	none	4	none	4	none
1 meter	9	none	14	none	3	none
1½ meter	9	1	3	none	5	none
2 meter	14	none	11	2	9	none
2½ meter	8	1	11	3	10	none
3 meter	8	2	8	4	9	none
	52mm	4 joint	51mm	9 joint	40mm	0

Ioints	dragged	Records of
joinis	(mm)	Preliminary
		Result

Dovetail Joint	43mm		60mm		46mm		GMELINA
		6 joints		6 joints		0	detached
Mortise and	49mm		44mm		24mm		117 mm
Tenon Joint							
		3 joints		6 joints		0	9 joints
TOTAL	92mm	9	104mm	12	70mm	0	
		RECORD	S OF FIN	AL RESU	LT		
	GME	GMELINA		COCO		WHITE LAUAN	
Joints	dragged (mm)	detached	dragged (mm)	detached	dragged (mm)	detache đ	
Dovetail Joint	67mm		43mm		58mm		168 mm
		5 joints		0		1 joint	6 joints
Mortise and Tenon Joint	52mm		51mm		40mm		143 mm
		4 joint		9 joint		0	13 joints
TOTAL	119mm	9	94mm	9	98mm	1	
GRAND	211 mm	18 joints	202	21 joints	163	1	
TOTAL		•	mm		mm	Joint	

	SUMMAR	Y RESULT (ON THE PE	RFORMAN	CE OF WOOL)
	GMELINA		coco		WHITE LAUAI	V
	dragged	detached	dragged	detached	dragged	detached
TOTAL	211 mm	18 joints	202 mm	21 joints	163 mm	1 joint

SUMMARY RESULT ON THE PERFORMANCE OF JOINTS								
	Preliminary Test	Final Test	TOTAL					
Dovetail Joint								
Dragged (mm)	149 mm	168 mm	317 mm					
Detached	12 joints	6 joints	18 joints					
Mortise and Tenon Joint								
Dragged (mm)	117 mm	143 mm	260 mm					
Detached	9 joints	13 joints	22 joints					



Republic of the Philippines NORTHWEST SAMAR STATE UNIVERSITY Main Campus, Calbayog City

AS-BAO FORM-B No. 2020-02

O.R. No. 3119995A

Date Tested: FEBRUARY 5, 2020

PRELIMINARY AND FINAL OBSERVATION IN COMPRESSION PARALLEL TO GRAIN

PRELIMINARY TEST RESULT ON WOOD SAMPLES

Sample ID	Width 1	Width 2	Area	Indicated	Compressive	Remarks
	(mm)	(mm)		Maximum	Strength	
				Load(kN)	(Mpa)	
GMELINA Sample 1	43	50	2150	59.1	27.5	
COCO Sample 2	41	51	2091	52.1	24.9	
WHITE LAUAN Sample 3	43	52	2236	37.5	16.8	
		x-x-x-Nothing	Follows-x-	-X-X		

AS-BAO FORM-B No. 2020-02

O.R. No. 3119995A

Date Tested: MARCH 24,2020

			0			
Sample ID	Width 1	Width 2	Area	Indicated	Compressive	Remarks
	(mm)	(mm)		Maximum	Strength	
				Load(kN)	(Mpa)	
GMELINA Sample 1	40	51	2040	59.4	29.1	
COCO Sample 2	43	52	2236	34.6	15.5	
WHITE LAUAN Sample	41	51	2091	52.5	25.1	
3						
		x-x-x-Nothing	Follows-x	-X-X		



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AS-BAO FORM-B No. 2020-02

O.R. No. 3119995A

Date Tested: FEBRUARY 5, 2020

PRELIMINARY AND FINAL OBSERVATION IN COMPRESSION PERPENDICULAR TO GRAIN

PRELIMINARY TEST RESULT ON WOOD SAMPLES

PREL	IIVIIIVAR I	IEST NES	JET ON	WOOD OAW		
Sample ID	Width 1	Width 2	Area	Indicated	Compressive	Remarks
	(mm)	(mm)		Maximum	Strength	
	()			Load(kN)	(Mpa)	
GMELINA Sample 1	46	52	2392	18.0	7.5	
COCO Sample 2	50	4.9	2450	8.9	36.3	
WHITE LAUAN Sample	45	50	2250	46.1	20.5	
3						
		x-x-x-Nothing	Follows-x-	-X-X		

AS-BAO FORM-B No. 2020-02

O.R. No. 3119995A

Date Tested: MARCH 24, 2020

Sample ID	Width 1	Width 2	Area	Indicated	Compressive	Remarks
Cumpio 15	(mm)	(mm)		Maximum	Strength	
				Load(kN)	(Mpa)	
GMELINA Sample 1	45	51	2295	52.1	22.7	
COCO Sample 2	45	50	2250	40.9	18.2	
WHITE LAUAN Sample	46	50	2300	10.5	4.6	
3		x-x-x-Nothing	Follows-x	-X-X		



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AS-BAO FORM-B No. 2020-02

O.R. No. 3119995A

Date Tested: FEBRUARY 5, 2020

PRELIMINARY AND FINAL OBSERVATION IN BENDING AND TENSION PARALLEL TO GRAIN

PRELIMINARY TEST RESULT ON WOOD SAMPLES

Sample ID	Width 1	Width 2	Length	Indicated	Bending/Ten	Remarks
	(mm)	(mm)	(m)	Maximum	sile	
				Load(kN)	Strength(Mp	
					a)	
GMELINA Sample 1	47	51	0.23	14.895	42.0	
COCO Sample 2	40	45	0.23	1.7	7.4	
WHITE LAUAN Sample	46	51	0.24	10.3	31.0	
3						
	X-X-	X- NOTHING	FOLLOWS	-X-X-X		

AS-BAO FORM-B No. 2020-02

O.R. No. 3119995A

Date Tested: MARCH 24, 2020

F.	INAL IES	KLOULI	OIA AAOC	JU SAMI LL	γ	
Sample ID	Width 1	Width 2	Length	Indicated	Bending/Ten	Remarks
	(mm)	(mm)	(m)	Maximum	sile	
				Load(kN)	Strength(Mp	
					a)	
GMELINA Sample 1	47	51	0.24	9.0	26.5	
COCO Sample 2	46	52	0.24	5.2	15.1	
WHITE LAUAN Sample	46	51	0.24	10.3	31.0	
3					L	
	X-X-	X- NOTHING	G FOLLOWS	S –X-X-X		



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AS-BAO FORM-B No. 2020-02 O.R. No. 3119995A

Date Tested: FEBRUARY 5, 2020

PRELIMINARY AND FINAL OBSERVATION IN SHEAR TEST PERPENDICULAR TO GRAIN

PRELIMINARY TEST RESULT ON WOOD SAMPLES

Sample ID	Area (mm²)	Indicated	Shear Strength	Remarks
		Maximum	(Mpa)	
		Load(kN)		
GMELINA Mortise &Tenon	1147	8.6	7.5	
Joint				
GMELINA Dovetail Joint	357	10.9	30.4	
COCO Mortise &Tenon Joint	1150	2.5	2.1	
COCO Dovetail Joint	402	1.0	2.6	
WHITE LAUAN Mortise	899.04	3.1	3.5	
&Tenon Joint				
WHITE LAUAN Dovetail Joint	548.38	2.7	4.9	
	x-x-x-x-Nothi	ng Follows-x-x-x-x		

AS-BAO FORM-B No. 2020-02

O.R. No. 3119995A

Date Tested: MARCH 24, 2020

Sample ID	Area (mm²)	Indicated Maximum Load(kN)	Shear Strength (Mpa)	Remarks
GMELINA Mortise &Tenon Joint	899.04	7.3	8.1	

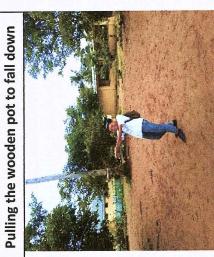
GMELINA Dovetail Joint	748.38	9.8	13.1	
COCO Mortise & Tenon Joint	1148	8.7	7.6	
COCO Dovetail Joint	410	8.1	19.8	
WHITE LAUAN Mortise & Tenon Joint	1147	5.3	4.6	
WHITE LAUAN Dovetail Joint	320	9.7	30.3	

PRELIMINARY AND FINAL PHOTO DOCUMENTATION ON IMPACT TESTING OF DOVETAIL JOINTS AND MORTISE AND TENON APPENDIX F JOINTS

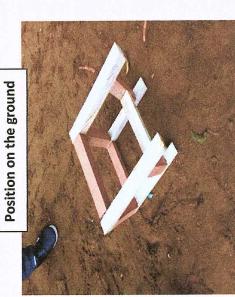
APPENDIX F-1

Preliminary Photo documentation on Impact Testing of Dovetail joints without the Aid of Nail or Wood Glue











APPENDIX F-2

Final Photo documentation on Impact Testing of Mortise and Tenon Joints without the Aid of Nail or Wood Glue



Position on the ground





Taking and recording the joint position



PRELIMINARY AND FINAL PHOTO OBSERVATION NOTES ON IMPACT TESTING OF DOVETAIL JOINTS AND MORTISE AND TENON JOINTS

PRELIMINARY OBSERVATIONAL NOTES IMPACT TEST ON WHITE LATIAN (MORTISE AND TENON IOINT)

		IMPACI IESI ON W	IMPACT TEST ON WHITE LADAN (MORTISE AND TENON JOINT)	AND IENON JOHN I)	
Height	No. of joint	7. HH.	EXTEND	EXTEND OF DAMAGES	
	Dragged/ Pulled-out/ruined	Uragged a little frDetached /Pulled	Uragged a little from its original position Detached /Pulled out from its original position	ion	
		Broken/Ruined jc	oint		
		Joint 1	Joint 2	Joint 3	Joint 4
½ meter	1	2mm			
		Dragged a little from its original position			
1 meter	1				
1 ½ meter	2	4mm Dragged a little from its original position	5mm Dragged a little from its original position		
2 meter	4	3mm	3mm	4mm	2mm
		Dragged a little from its original position	Dragged a little from its original position	Dragged a little from its original position	Dragged a little from its original position
2 ½ meter	4	5mm Dragged a little from its original position	3mm Dragged a little from its original position	5mm Dragged a little from its original position	5mm Dragged a little from its original position
3 meter	4	8mm Dragged a little from its original position	5mm Dragged a little from its original position	4mm Dragged a little from its original position	6mm Dragged a little from its original position

FINAL OBSERVATIONAL NOTES IMPACT TEST ON WHITE LAUAN (MORTISE AND TENON JOINT)

Dragged/Pulled • Detached / Pulled out from its original position • Broken/Ruined joint Joint 1	Height	No. of joint		EXTEND	EXTEND OF DAMAGES	
Dragged a little from its Dragged a little from original position Dragged a little from its Original position Dragged a little from its Original position Dragged a little from its Dragged a little from original position Dragged a little from its Original position		Dragged/Pulled- out/ruined	Dragged a little frDetached /PulledBroken/Ruined ic	com its original position out from its original posi	tion	
Dragged a little from its Dragged a little from original position its original position and original position original position its original position original position its original position its original position original position its original position original position its original pos						
Dragged a little from its original position original position its original position Dragged a little from its original position original position original position its original position original position its original position its original position its original position its original position original position its original position original position its original position original position its original position			Joint 1	Joint 2	Joint 3	Joint 4
Dragged a little from its original position 2	½ meter	2	4mm	3mm		
Dragged a little from its Dragged a little from original position 4 5mm Dragged a little from its original position original position its original position 4 9mm Dragged a little from its Dragged a little from original position its original position original position its original position			Dragged a little from its original position	Dragged a little from its original position		
Dragged a little from its original position 4 5mm Dragged a little from its Original position 4 9mm Dragged a little from its Original position 4 5mm Dragged a little from its Original position 4 5mm Dragged a little from its Original position 4 5mm Dragged a little from its Original position its original position	1 meter	2	3mm	3mm		
Dragged a little from its original position original position original position its original position			Dragged a little from its original position	Dragged a little from its original position		
Dragged a little from its original position its original position 4 9mm 6mm Dragged a little from its original position original position 4 2mm Dragged a little from its original position original position its original position its original position its original position original position its original position	1 1/2 meter	4	5mm	3mm	3mm	3mm
Dragged a little from its Dragged a little from original position 4			Dragged a little from its original position	Dragged a little from its original position	Dragged a little from its original position	Dragged a little from its original position
Dragged a little from its original position original position 4	2 meter	4	9mm	emm 9	5mm	mm9
Dragged a little from its Dragged a little from original position 4 9mm Dragged a little from its Original position its original position its original position its original position			Dragged a little from its original position	Dragged a little from its original position	Dragged a little from its original position	Dragged a little from its original position
Dragged a little from its original position Dragged a little from its original position its original position its original position	2 ½ meter	4	2mm	5mm	10mm	1mm Transport of 11H of from its
9mm 7mm Dragged a little from its Dragged a little from orioinal position its orioinal position			Dragged a nute from its original position	Dragged a little from its original position	Dragged a mue from us original position	original position
Dragged a little from its original position	3 meter	4	9mm	7mm	6mm	6mm
			Dragged a little from its original position	Dragged a little from its original position	Dragged a little from its original position	Dragged a little from its original position

PRELIMINARY OBSERVATIONAL NOTES IMPACT TEST ON WHITE LAUAN (DOVETAIL JOINT)

OF DAMAGES	Joint 3 Joint 4 Joint 5	2mm 2mm Dragged a little from its original position	4mm2mmDragged a little from its original positionDragged a little from its original position	Imm Imm Dragged a little from Dragged a little from its original position its original position	3mm 3mm Dragged a little from its original position	4mm2mmDragged a little fromDragged a little fromDragged a littleits original positionfrom its original position	Dragged a little from Dragged a little from its original position its original position position
its original posi	Joint 2	4mm Dragged a little from Its original position	4mm Dragged a little from Its original position	4mm Dragged a little from Its original position	3mm Dragged a little from lits original position	4mm Dragged a little from lits original position	6mm Dragged a little from its original position
ed a	Joint 1	10mm Dragged a little from its original position	15mm Dragged a little from its original position	4mm Dragged a little from its original position	detached	10mm Dragged a little from its original position	16mm Dragged a little from its original position
No. of joint Dragged/ Pulled- out/ruined		4	ഹ	4	4	സ	rv.
Height		½ meter	1 meter	1 ½ meter	2 meter	2 ½ meter	3 meter

FINAL OBSERVATIONAL NOTES IMPACT TEST ON WHITE LAUAN (DOVETAIL JOINT)

• Detached / Pulled out fit • Broken/Ruined joint 5mm Dragged a little from little from shorition 6mm Dragged a Dragged a Little from little littl	Height	No. of joint Dragged/Pulled-	Dragged a		EX. little from its original position	EXTEND OF DAMAGES ition	DAMAGES			
Joint 1 Joint 2 Joint 3 Joint 4 1 5mm 1 1 Dragged a little from its original position 3mm 2mm 2mm 3 6mm 3mm 2mm 2mm 4 4mm 4mm 2mm 2mm 4 4mm 4mm 2mm 2mm 15 original position 12 original position 12 original position 12 original position 12 mm 8 15 mm 7mm 6mm 7mm Bragged a position 12 mm 7mm 12 mm Bragged a position 15 original position 15 original position 15 original position Bragged a position 15 mm 15 original position 15 original position Bragged a pragged a position 15 original position 15 original position 15 original position		out/ruined	DetaclBroke	hed /Pulled o n/Ruined join	ut from its origin t	nal position				
1 5mm Dragged a little from its original position 4 A Amm Dragged a little from little from its original position By Dragged a Dragged a Dragged a little from little from little from its original position A Amm Dragged a Dragged a Dragged a Dragged a little from little from its original position By Dragged a Dragged a Dragged a Dragged a little from little from its original its original its original its original position By T5mm T7mm T7mm Tmm Oragged a Dragged a Dragged a little from its little from its original its original its original little from little lit										
1 Dragged a little from its original position 3 Gmm 3mm 2mm 2mm 2mm little from little from little from little from is original position position position position little from little fr			Joint 1	Joint 2	Joint 3	Joint 4	Joint 5	Joint 6		
Dragged a little from its original position 3mm 2mm	1/2	1	5mm							
its original 3 6mm 3mm 2mm Dragged a Dragged a Dragged a little from little from little from its original position 4 4 4mm 4mm 2mm 2mm Dragged a Dragged a Dragged a little from little littl	meter		Dragged a							
its original 3 6mm 3mm 2mm 2mm 2mm Dragged a little from its original position 4 4 4mm Dragged a little from its original position 8 15mm Dragged a Dragged a Dragged a little from its original position positio			little from							
36mm3mm2mmDragged a little from positionDragged a little from positionDragged a little from positionDragged a positionDragged a position44mm4mm2mmDragged a little from positionDragged a little from positionDragged a 			its original							
36mm3mm2mmDragged a little from its original DositionDragged a little from positionDragged a positionDragged a Dragged aDragged a Dragged a little from positionDragged a little from positionDragged a little from positionDragged a little from positionDragged a little from positionDragged a position815mm7mm6mm7mmBragged a little from little from little fromDragged a little from little from little fromJittle from little from little from little fromJittle from little from little from little from little fromJittle from little from little from little fromJittle from little from little from little fromJittle from little from little from little from			position							
Dragged a Dragged a Dragged a little from its its original position position position Dragged a Dragged a Dragged a Dragged a Dragged a Dragged a little from its original position pragged a little from	1	3	mm9	3mm	2mm					
its original its original original position position position Amm Amm Zmm Zmm Zmm Dragged a Dragged a Diragged a little from little from little from its original position position position Dragged a Dragged a Dragged a Dragged a little from littl	meter		Dragged a	Dragged a	Dragged a					
4 4mm 4mm 2mm 2mm Dragged a little from its original position Dragged a little from little from its original position Dragged a little from little from its original position Dragged a little from			little from	little from	little from its					
4 4mm 4mm 2mm 2mm 2mm 2mm 2mm 2mm 2mm 2m			its original	its original	original					
4 4mm 4mm 2mm 2mm 2mm 2mm Dragged a Dragged a Dragged a Ittle from little from little from its original position position position 7mm 6mm 7mm Dragged a Dragged a Dragged a Dragged a little from little from little from little from little from its original			position	position	position					
Dragged a Dragged a Dragged a Dragged a little from little from little from little from its original position position position position from Dragged a Dragged a little from	1 1/2	4	4mm	4mm	2mm	2mm				
its original its original original its original position position 8 15mm	meter		Dragged a	Dragged a	Dragged a	Dragged a				
its originalits originalits originalits originalpositionpositionpositionposition815mm7mm6mm7mmDragged aDragged aDragged aDragged alittle fromlittle fromlittle fromlittle fromits originalits originalits original			little from	little from	little from its	little from				
815mm7mm6mm7mmDragged aDragged aDragged aDragged aIttle from little from its originalIttle from its original			its original	its original	original	its original				
815mm7mm6mm7mmDragged aDragged aDragged aDragged alittle fromlittle fromlittle fromlittle fromits originalits originalits original			position	position	position	position				
Dragged a Dragged a Dragged a Dragged a little from little from its original its original original lits original	2	80	15mm	7mm	mm9	7mm	8mm	7mm	3mm	4mm
little from little from its little from its original	meter		Dragged a	Dragged a	Dragged a	Dragged a	Dragged a	Dragged a	Dragged a	Dragged a
its original original its original			little from	little from	little from its	little from	little from	little from	little from	little from
			its original	its original	original	its original	its original	its original	its original	its original
position			position	position	position	position	position	position	position	position

4mm	Dragged a	little from		position					
5mm	Dragged a	little from	its original	position	2mm	Dragged a		-==	position
5mm	Dragged a	little from its	original	position	4mm	Dragged a	little from its	original	position
4mm	Dragged a	little from	its original	position	4mm	Dragged a	little from	its original	position
3mm	Dragged a	little from	its original	position	8mm	Dragged a	little from	its original	position
5					4				
2 1/2	meter				3	meter			

PRELIMINARY OBSERVATIONAL NOTES IMPACT TEST ON COCO (MORTISE AND TENON JOINT)

Joint 1 Joint 2 Joint 3 Joint 4 Joint 5 Joint 6 Joint 7 Joint 8 Join	Height	No. of joint Dragged/ Pulled- out/ruined	Dragged aDetached /Broken/Ru		EXTEND OF DAMAGES little from its original position Pulled out from its original position ined joint	osition				
Tittle from its little from its original origina			Joint 1	Joint 2	Joint 3	Joint 4	Joint 5	Joint 6	Joint 7	
little from its little fro	½ meter	೮	1mm Dragged a	2mm Dragged a	2mm Dracoed a					
original original original original position position position Amm 5mm 2mm 6 6mm 6mm Dragged a Ittle from its Ittle from its <t< td=""><th></th><td></td><td>little from its</td><td>little from its</td><td>little from its</td><td></td><td></td><td></td><td></td><td></td></t<>			little from its	little from its	little from its					
6 6mm 6mm 2mm 4mm 5mm 2mm 2mm 2mm 2mm original Dragged a			original position	original position	original position					
Dragged a Dragged a Dragged a little from its original Dragged a Dragged a little from its original Dragged a little from its original Inttle from its original	1 meter	9	6mm	mm9	2mm	4mm	5mm	2mm	2mm	
little from its little from its original origina			Dragged a	Dragged a	Dragged a	Dragged a	Dragged a	Dragged a	Dragged a	
original original original original original its original its original position 7			little from its	little from its	little from its	little from its	little from	little from	little from	
7 3mm 2mm 1mm 2mm 5mm 5mm Dragged a Doriginal position Dragged a D			original	original	original	original	its original	its original	its original	
73mm2mm1mm2mm5mmDragged a little from its original bositionDragged a original positionDragged a original original bositionDragged a original original original bositionlittle from its original bositionlittle from its positionlittle from its positionlittle from its positionDragged a positionDragged a positionDragged a positionDragged a positionDragged a positionBurm8detached detached9mm1mm8mmBragged a Dragged a 			position	position	position	position	position	position	position	
Dragged a Dragged a Dragged a Dragged a Dragged a Dragged a little from its little from its original original original original original original its original its original original original original original original its original its original ori	1 1/2	7	3mm	2mm	1mm	2mm	5mm	5mm		
little from its little from litt	meter		Dragged a	Dragged a	Dragged a	Dragged a	Dragged a	Dragged a		
6 detached 6mm 14mm 6mm 9mm 1 Dragged a Dragged a Dragged a Dragged a Dragged a 1 Ittle from its 1 position position position position 8 detached detached Dragged a Dragged a 1 Ittle from its Itmm 8mm 1 Dragged a Dragged a 1 Ittle from its Ittle from its			little from its	little from its	little from its	little from its	little from	little from		
6 detached bosition position position position position position position 6 detached bragged a Dragged a Dragged a Dragged a Dragged a little from its little from bosition position Dragged a Dragged a Bragged a Bragged a Dragged a Dragged a Dragged a little from its little f			original	original	original	original	its original	its original		
6 detached 6mm 14mm 6mm 9mm Dragged a Dragged a Dragged a Dragged a Dragged a little from its little from its little from its little from its original original its original position position position 8 detached 9mm 1mm 8mm Bragged a Dragged a Dragged a Dragged a little from its little from its little from			position	position	position	position	position	position		
Dragged a Little from its little from its original original original position position position position position Dragged a Dragged a Dragged a Dragged a Intle from its little from its little from its original i	2 meter	9	detached	mm9	14mm	emm	9mm	9mm		
little from its original original its original original its original position position Dragged a				Dragged a	Dragged a	Dragged a	Dragged a	Dragged a		
8 detached detached 9mm 1mm 8mm Dragged a Dragged a Dragged a Dragged a Ittle from its Ittle from				little from its	little from its	little from its	little from	little from		
8detachedpositionpositionpositionposition8detached9mm1mm8mmDragged aDragged aDragged aDragged alittle from itslittle from itslittle from its				original	original	original	its original	its original		
8 detached 9mm 1mm 8mm Dragged a Dragged a Dragged a Dragged a little from its little from its little from				position	position	position	position	position		
Dragged a Dragged a Dragged a Ittle from its little from	2 1/2	0 0	detached	detached	9mm	1mm	8mm	4mm		
little from its little from	meter				Dragged a	Dragged a	Dragged a	Dragged a		
					little from its	little from its	little from	little from		

	2mm Dragged a little from its original position
	6mm Dragged a little from its original position
its original position	8mm Dragged a little from its original position
its original its original position	1mm Dragged a little from its original position
original position	4mm Dragged a little from its original position
original position	detached
	detached
	detached
	∞
	3 meter

FINAL OBSERVATIONAL NOTES IMPACT TEST ON COCO (MORTISE AND TENON JOINT)

Cint	JOINT 0																		in the same		
T tuin 7) June /																				
To:o1	o mirof																				
) Juint 3				2mm	Dragged	a little	from its	original	position	3mm	Dragged	a little	from its	original	position					
osition Loint 4	Joint 4				4mm	Dragged a	little from its	original	position		3mm	Dragged a	little from its	original	position		11mm	Dragged a	little from its	original	position
EXTEND OF DAMAGES Dragged a little from its original position Broken/Ruined joint	Joint 3				5mm	Dragged a	little from its	original	position		2mm	Dragged a	little from its	original	position		3mm	Dragged a	little from its	original	position
EXTEND OF Dragged a little from its Detached /Pulled out fr Broken/Ruined joint	Joint 2	2mm Dragged a li#le from	its original	position	9mm	Dragged a	little from	its original	position		2mm	Dragged a	little from	its original	position		detached				
• Dragged • Detached • Broken/	Joint 1	4mm Dragged a little from its	original	position	14mm	Dragged a	little from its	original	position		detached						detached				
No. of joint Dragged/Pulled- out/ruined		6			5						5						4				
Height		½ meter			1 meter						1 1/2	meter					2 meter				

					-						
						5mm	Dragged	a little	from its	original	position
4mm	Dragged	a little	from its	original	position	3mm	Dragged	a little	from its	original	position
						8mm	Dragged	a little	from its	original	nosition
7mm	Dragged a	little from its	original	position		detached					
detached						detached					
detached						detached					
detached						detached					
9						7					
2 1/2	meter					3 meter					

PRELIMINARY OBSERVATIONAL NOTES IMPACT TEST ON COCO (DOVETAIL JOINT)

Toint 9	JOHN																					
Toint	Journe																					
Toint 7	JOHN /					7mm	Dragged	a little	from its	original	- Contract						6mm	Dragged	a little	from its	original	position
Toint 6	Journ 0					3mm	Dragged	a little	from its	original	TOTAL COLOR						14mm	Dragged	a little	from its	original	position
Loint R	Joint					4mm	Dragged a	little from	its original	position							8mm	Dragged a	little from	its original	position	•
Sition Solition	JOINT 4					8mm	Dragged a	little from	its original	position	3mm	Juliul G	Dragged a	little from	its original	position	1mm	Dragged a	little from	its original	position	•
EXTEND OF DAMAGES from its original position d out from its original position is original position.	JOHNES					4mm	Dragged a	little from its	original	position	13mm	1. C	Dragged a	little from its	original	position	2mm	Dragged a	little from its	original	position	
EXTEND OF DAMAGES Dragged a little from its original position Detached /Pulled out from its original position Broken/Ruined joint	JOIIIL 2	2mm	Dragged a little from its	original	position	10mm	Dragged a	little from its	original	position	11mm	Timini G	Dragged a	little from its	original	position	2mm	Dragged a	little from its	original	position	.
• Dragged • Detache • Broken/	JOINT 1	2mm	Dragged a little from its	original	position	deatched					mmy	omimo &	Dragged a	little from its	original	position	detached					
No. of joint Dragged/ Pulled- out/ruined		7				7					-	H					7					
Height		½ meter				1 meter					1 1%	7/ 1	meter				2 meter					

mm9	Sec. 10.		from its		position							
mm9	Dragged	a little	from its	original	position	1mm	Dragged	a little	from its	original	position	
9mm	Dragged a	little from	its original	position		11mm	Dragged a	little from	its original	position		
10mm	Dragged a	little from	its original	position		9mm	Dragged a	little from	its original	position		
detached						9mm	Dragged a	little from its	original	position		
detached						detached						
detached						detached						
7						9						
2 1/2	meter					3 meter						

FINAL OBSERVATIONAL NOTES IMPACT TEST ON COCO (DOVETAIL JOINT)

gged achee	Dragged Detachee Broken/ Smm Smm Dragged a little from its original position 6mm Dragged a little from its original position Amm Dragged a little from its original its original its original its original its original its original its position its original
Smm 7mm	
Dragged a	Dragged a
original its original	its original its original
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
position position position	20011000

4mm Dragged a little from its original position	
5mm Dragged a little from its original position	2mm Dragged a little from its original position
5mm Dragged a little from its original position	4mm Dragged a little from its original position
4mm Dragged a little from its original position	4mm Dragged a little from its original position
3mm Dragged a little from its original position	8mm Dragged a little from its original position
гo	4
2 ½ meter	3 meter

PRELIMINARY OBSERVATIONAL NOTES IMPACT TEST ON GMELINA (MORTISE AND TENON JOINT)

ıırgıarı	No. of joint Dragged/ Pulled- out/ruined	Dragged a 1Detached / /Broken/Rui	EXTEND O. Dragged a little from its Detached / Pulled out fi Broken/Ruined joint	EXIEND OF DAMAGES ittle from its original position Pulled out from its original position ined joint	osition				
		Joint 1	Joint 2	Joint 3	Joint 4	Joint 5	Joint 6	Joint 7	Joint 8
½ meter	0								and the second s
1 meter	1	mm9							
		Dragged a							
		little from its							
		original position							
1 1/2	9	detached	detached	16mm	13mm	mm9	emm9		
meter				Dragged a	Dragged a	Dragged a	Dragged a		
				little from its	little from its	little from	little from		
				original	original	its original	its original		
				position	position	position	position		
2 meter	4	3mm	10mm	8mm	4mm				
		Dragged a	Dragged a	Dragged a	Dragged a				
		little from its	little from its	little from its	little from its				
		original	original	original	original				
		position	position	position	position				
2 1/2	8	4mm	4mm	4mm	4mm	2mm	2mm	2mm	2mm
meter		Dragged a	Dragged a	Dragged a	Dragged a	Dragged a	Dragged a	Dragged a	Dragged a
		little from its	little from its	little from its	little from its	little from	little from	little from	little from
		original	original	original	original	its original	its original	its original	its original
		position	position	position	position	position	position	position	position
3 meter	7	detached	10mm	10mm	13mm	13mm	emm9	7mm	

Dragged a	Dragged a	Dragged a	Dragged a	Dragged a	Dragged a	
little from its	little from its	little from its	little from	little from	little from	
original	original	original	its original	its original	its original	
position	position	position	position	position	position	

FINAL OBSERVATIONAL NOTES IMPACT TEST ON GMELINA (MORTISE AND TENON JOINT)

Height	No. of joint			DAMAGES					
	Dragged/Pulled- out/ruined	DraggedDetachecBroken/	Dragged a little from its original position Detached /Pulled out from its original position Broken/Ruined joint	original position m its original pos	ition				
		Joint 1	Joint 2	Joint 3	Joint 4	Joint 5	Joint 6	Joint 7	Joint 8
	1	4mm							
		Dragged a							
		original							
1	2	7mm	9mm						
		Dragged a	Dragged a						
		little from its	little from its						
		original	original						
		position	position						
	9	detached	5mm	7mm	9mm	5mm	3mm		
			Dragged a	Dragged a	Dragged a	Dragged	Dragged		
			little from its	little from its	little from its	a little	a little		
			original	original	original	from its	from its		
			position	position	position	original	original		
						position	position		
	4	9mm	14mm	11mm	10mm				
		Dragged a	Dragged a	Dragged a	Dragged a				
		little from its	little from its	little from its	little from its				
		original	original	original	original				
		position	position	position	position				

4mm	Dragged	a little	from its	original	position	mm6	Dragged	a little	from its	original	position
3mm	Dragged	a little	from its	original	position	8mm	Dragged	a little	from its	original	position
5mm	Dragged a				22	9mm	Dragged a	little from its	original	position	
mm9	Dragged a	little from its	original	position		10mm	Dragged a	little from its	original	position	
8mm	Dragged a	little from its	original	position		detached					
detached						detached					
9						9					
2 1/2	meter	011				3 meter					

PRELIMINARY OBSERVATIONAL NOTES IMPACT TEST ON GMELINA (DOVETAIL JOINT)

Toint 8	Jorus																						
Ioint 7) Journal								de la composition della compos														
Toint	JOINT				The state of the s																		
Toint 5) June 2																			9mm	Dragged a	little from	
eS on Toint 4	Jount #									7mm	Dragged a little	from its	original	position	6mm	Dragged a little	from its	original	position	4mm	Dragged a little	from its	
EXTEND OF DAMAGES le from its original position lled out from its original position id joint	Joint 3				4mm	Dragged a little	from its original	position		8mm	Dragged a little	from its original	position		7mm	Dragged a little	from its original	position		6mm	Dragged a little	from its original	position
Dragged a little from its original position Detached /Pulled out from its original position Broken/Ruined joint	Joint 2	4mm Dragged a little	from its original	position	4mm	Dragged a little	from its original	position		10mm	Dragged a little	from its original	position		9mm	Dragged a little	from its original	position		detached			
Dragge Detach Broken Inint 1	Joint 1	Dragged a	little from its	original	15mm	Dragged a	little from its	original	position	7mm	Dragged a	little from its	original	position	detached					detached			
No. of joint Dragged/ Pulled- out/ruined		7			8					4					4					5			
Height	1/	½ meter			1 meter					1 1/2	meter				2 meter					2 1/2	meter		

	3mm	Dragged	a little	from its	original	position
	3mm	Dragged	a little	from its	original	position
its original position		Dragged a				
original position	12mm	Dragged a little	from its	original	position	
	10mm	Dragged a little	from its original	position		
	detached					
	detached					
	7					
	3 meter					

FINAL OBSERVATIONAL NOTES IMPACT TEST ON GMELINA (DOVETAIL JOINT)

	Joint 8																				
	Joint 7																				
	Joint 6																			18	
DAMAGES	Joint 5																8mm	Dragged a	little from	its original	position
EXTEND OF DAMAGES tition al position	Joint 4											2mm	Dragged a	little from	its original	position	2mm	Dragged a	little from	its original	position
EXTEND Dragged a little from its original position Detached /Pulled out from its original position Broken/Ruined joint	Joint 3						2mm	Dragged a	little from its	original	position	9mm	Dragged a	little from its	original	position	2mm	Dragged a	little from its	original	position
	Joint 2	2mm	Dragged a	little from	its original	position	2mm	Dragged a	little from	its original	position	10mm	Dragged a	little from	its original	position	detached				
Dragged a Detached / Broken/Ru	Joint 1	2mm	Dragged a	little from	its original	position	4mm	Dragged a	little from	its original	position	10mm	Dragged a	little from	its original	position	detached				
No. of joint Dragged/Pulled- out/ruined		2					3					4					5				
Height		1/2	meter				1	meter				1 1/2	meter				2	meter			

	4mm Dragged a little from its original position
15mm Dragged a little from its original position	4mm Dragged a little from its original position
8mm Dragged a little from its original position	4mm Dragged a little from its original position
8mm Dragged a little from its original position	10mm Dragged a little from its original position
10mm Dragged a little from its original position	detached
10mm Dragged a little from its original position	detached
detached	detached
9	7
2 ½ meter	3 meter

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